



Advanced Robotics

ENGG5402 Spring 2023



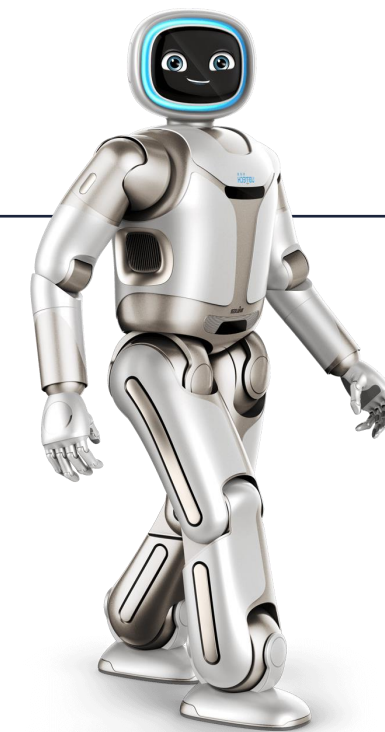
Fei Chen

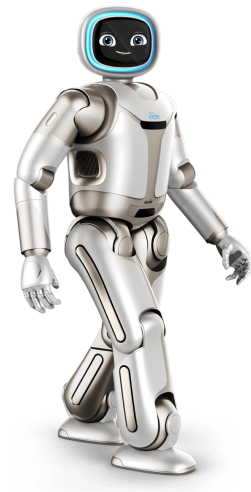
Topics:

- Euler and roll-pitch-yaw angles

Readings:

- Siciliano: Sec. 2.1-2.6, 2.10

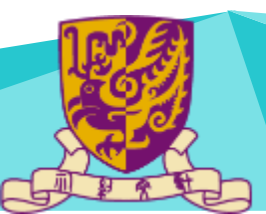


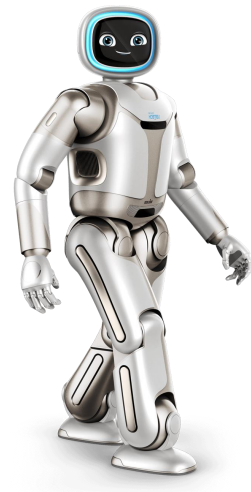


Outline

Euler and roll-pitch-yaw angles

- Basic Definitions

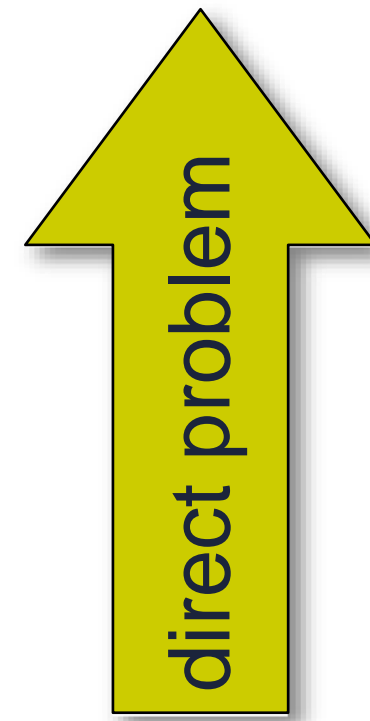




Basic Definitions

"Minimal" representation

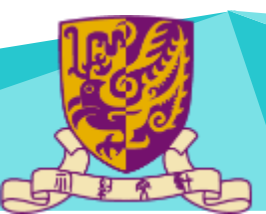
- rotation matrices:



- 9 elements
 - 3 orthogonality relationships
 - 3 unitary relationships
-
- = 3 independent variables

- sequence of 3 rotations w.r.t. independent axes
 - by angles $\alpha_i, i = 1, 2, 3$, around fixed (a_i) or moving/current (a'_i) axes
 - generically called Roll-Pitch-Yaw (fixed axes) or Euler (moving axes) angles
 - 12+12 possible different sequences (e.g., **XYX**)
 - without contiguous repetitions of axes (e.g., no **XXZ** nor **YZ'Z'**)
 - actually, only 12 sequences are different since we shall see that

$$\{(a_1, \alpha_1), (a_2, \alpha_2), (a_3, \alpha_3)\} \equiv \{(a'_3, \alpha_3), (a'_2, \alpha_2), (a'_1, \alpha_1)\}$$

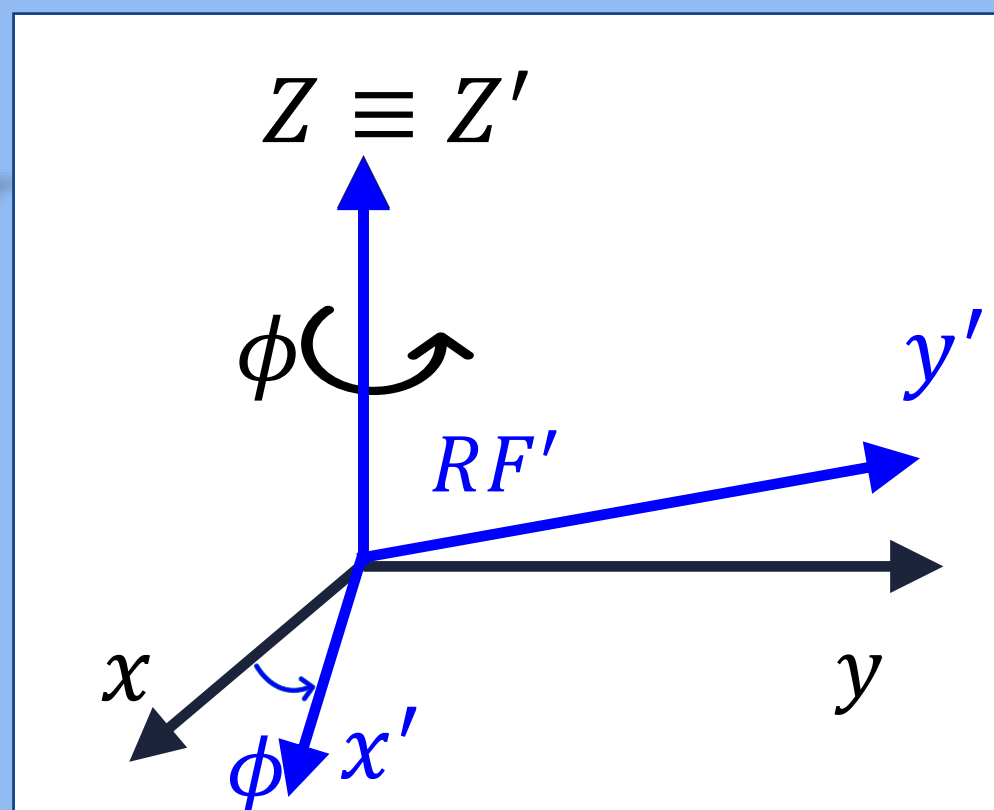




Basic Definitions

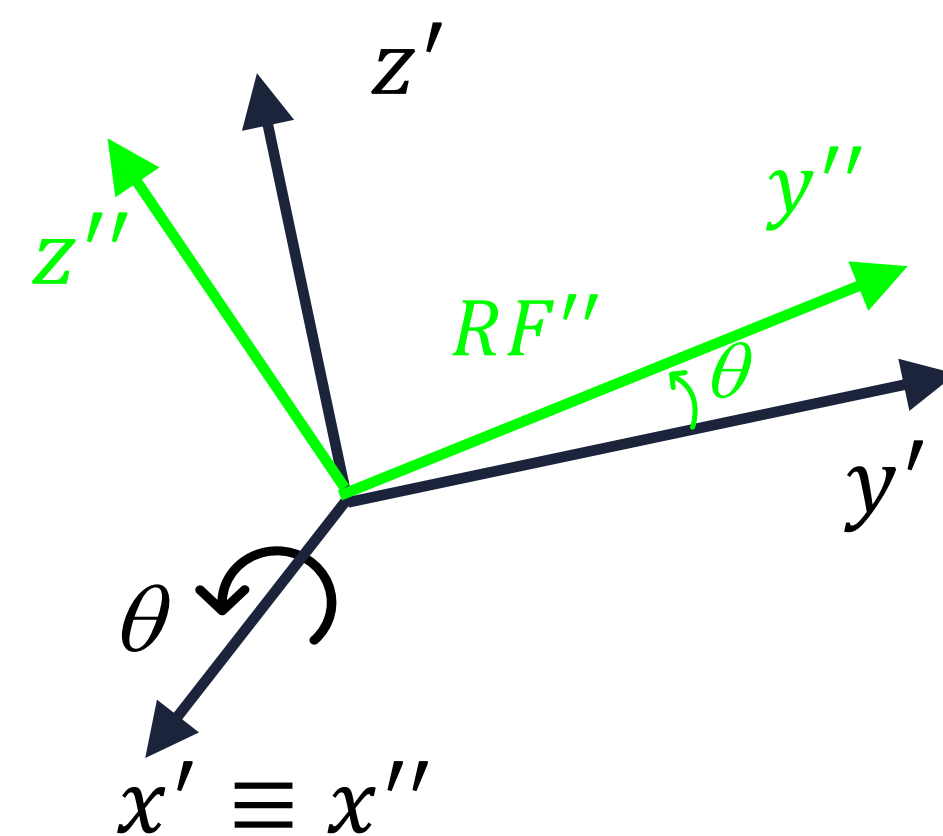
ZX'Z'' Euler angles

1



$$R_Z(\phi) = \begin{bmatrix} \cos \phi & -\sin \phi & 0 \\ \sin \phi & \cos \phi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

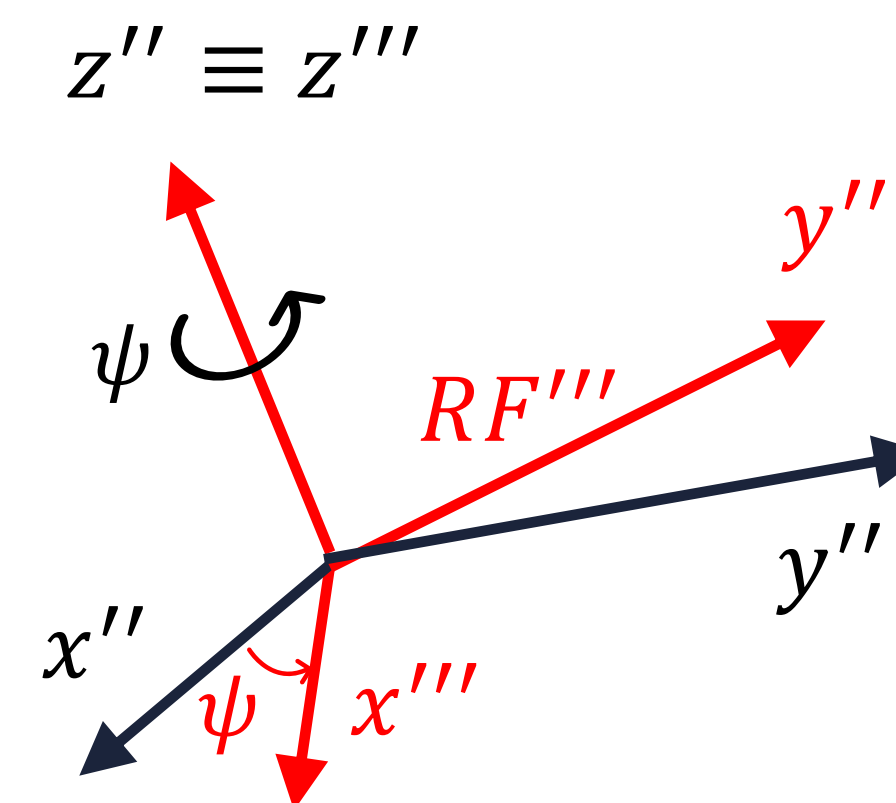
2

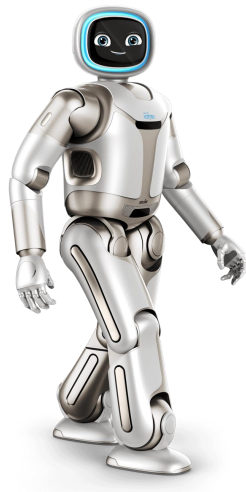


$$R_{X'}(\theta) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \theta & -\sin \theta \\ 0 & \sin \theta & \cos \theta \end{bmatrix}$$

3

$$R_{Z''}(\psi) = \begin{bmatrix} \cos \psi & -\sin \psi & 0 \\ \sin \psi & \cos \psi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$





Basic Definitions

ZX'Z'' Euler angles

- direct problem: given ϕ, θ, ψ , find R

$$R_{ZX'Z''}(\phi, \theta, \psi) = R_Z(\phi)R_{X'}(\theta)R_{Z''}(\psi)$$

order of definition
in concatenation

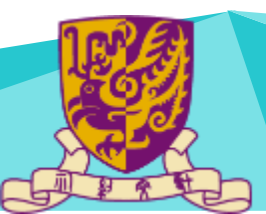
$$= \begin{bmatrix} c\phi c\psi - s\phi c\theta s\psi & -c\phi s\psi - s\phi c\theta c\psi & s\phi s\theta \\ s\phi c\psi + c\phi c\theta s\psi & -s\phi s\psi + c\phi c\theta c\psi & -c\phi s\theta \\ s\theta s\psi & s\theta c\psi & c\theta \end{bmatrix}$$

- given a vector $v''' = (x''', y''', z''')$ expressed in RF'' , its expression in the coordinates of RF is

$$v = R_{ZX'Z''}(\phi, \theta, \psi)v'''$$

- the orientation of RF is the same that would be obtained with the sequence of rotations

ψ around z , θ around x (fixed), ϕ around z (fixed)





Basic Definitions

ZX'Z'' Euler angles

- **inverse problem**: given $R = \{r_{ij}\}$, find ϕ, θ, ψ

$$\begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix} = \begin{bmatrix} c\phi c\psi - s\phi c\theta s\psi & -c\phi s\psi - s\phi c\theta c\psi & s\phi s\theta \\ s\phi c\psi + c\phi c\theta s\psi & -s\phi s\psi + c\phi c\theta c\psi & -c\phi s\theta \\ s\theta s\psi & s\theta c\psi & c\theta \end{bmatrix}$$

- if $r_{13}^2 + r_{23}^2 = s^2\theta$, $r_{33} = c\theta \Rightarrow$

$$\theta = \text{atan2} \left\{ \pm \sqrt{r_{13}^2 + r_{23}^2}, r_{33} \right\}$$

two values differing just for the sign

- if $r_{13}^2 + r_{23}^2 \neq 0$ (i.e., $s\theta \neq 0$)

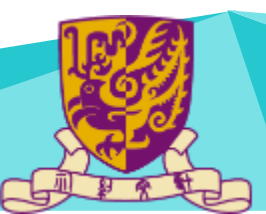
$$r_{31}/s\theta = s\psi, r_{32}/s\theta = c\psi \Rightarrow$$

$$\phi = \text{atan2} \{r_{13}/s\theta, -r_{23}/s\theta\}$$

- similarly...

$$\psi = \text{atan2} \{r_{31}/s\theta, r_{32}/s\theta\}$$

- there is always a **pair** of solutions in the regular case
- there are always **singularities** (here $\theta = 0$ **or** $\pm \pi$) \Rightarrow only the **sum** $\phi + \psi$ **or** the **difference** $\phi - \psi$ can be determined



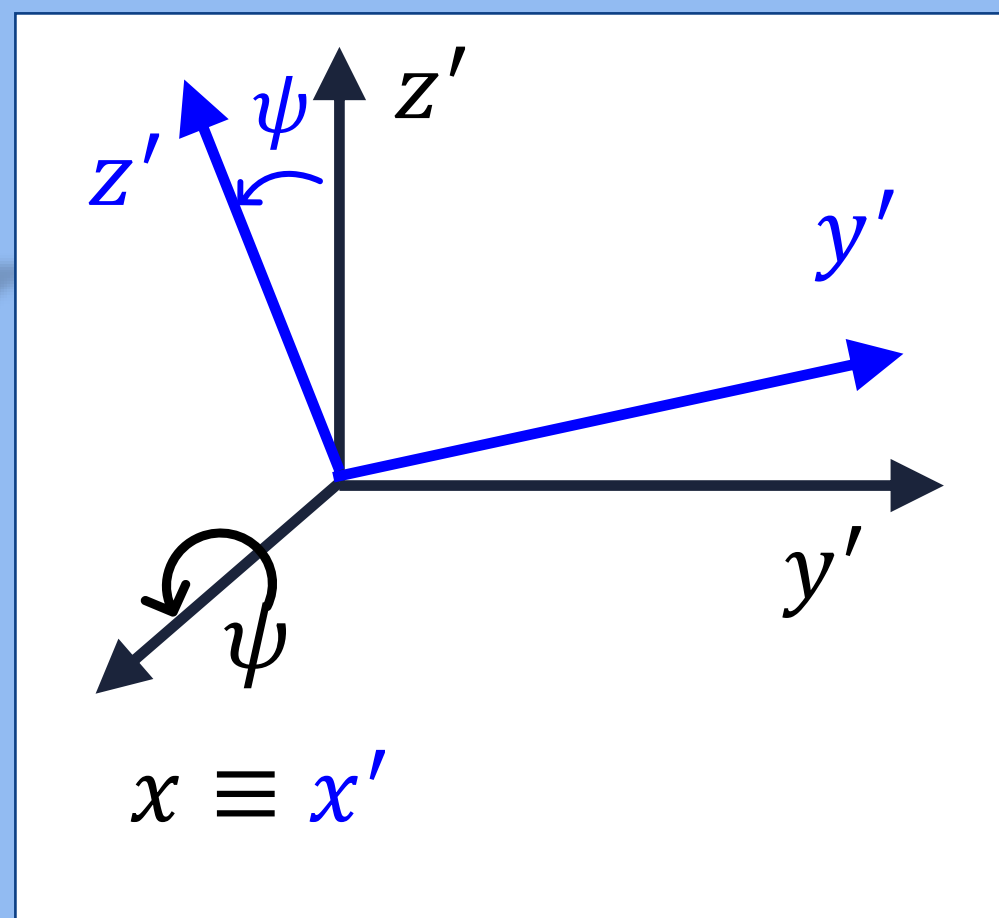


Basic Definitions

Roll-Pitch-Yaw angles(fixed XYZ)

ROLL

1



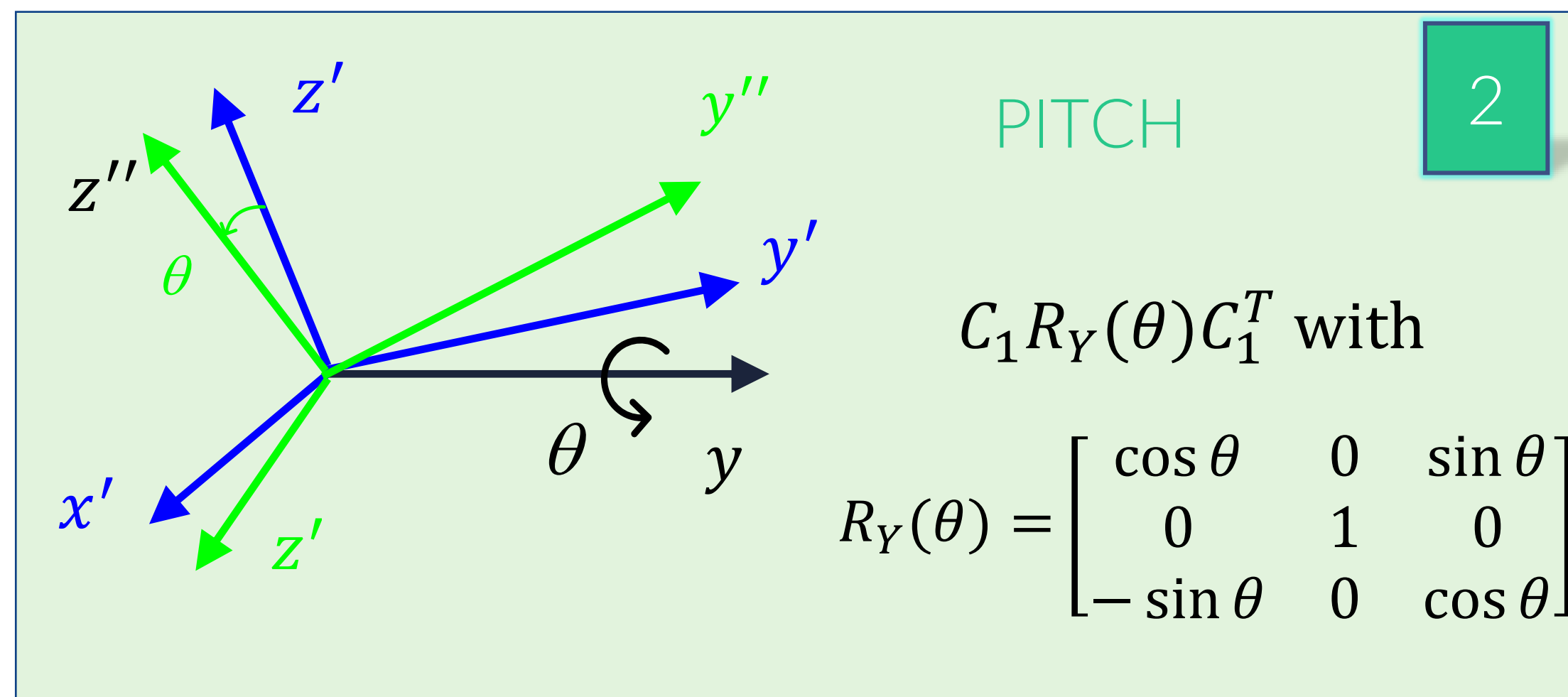
$$R_X(\psi) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \psi & -\sin \psi \\ 0 & \sin \psi & \cos \psi \end{bmatrix}$$

$$C_2 R_Z(\phi) C_2^T$$

$$\text{with } R_Z(\phi) = \begin{bmatrix} \cos \phi & -\sin \phi & 0 \\ \sin \phi & \cos \phi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

PITCH

2

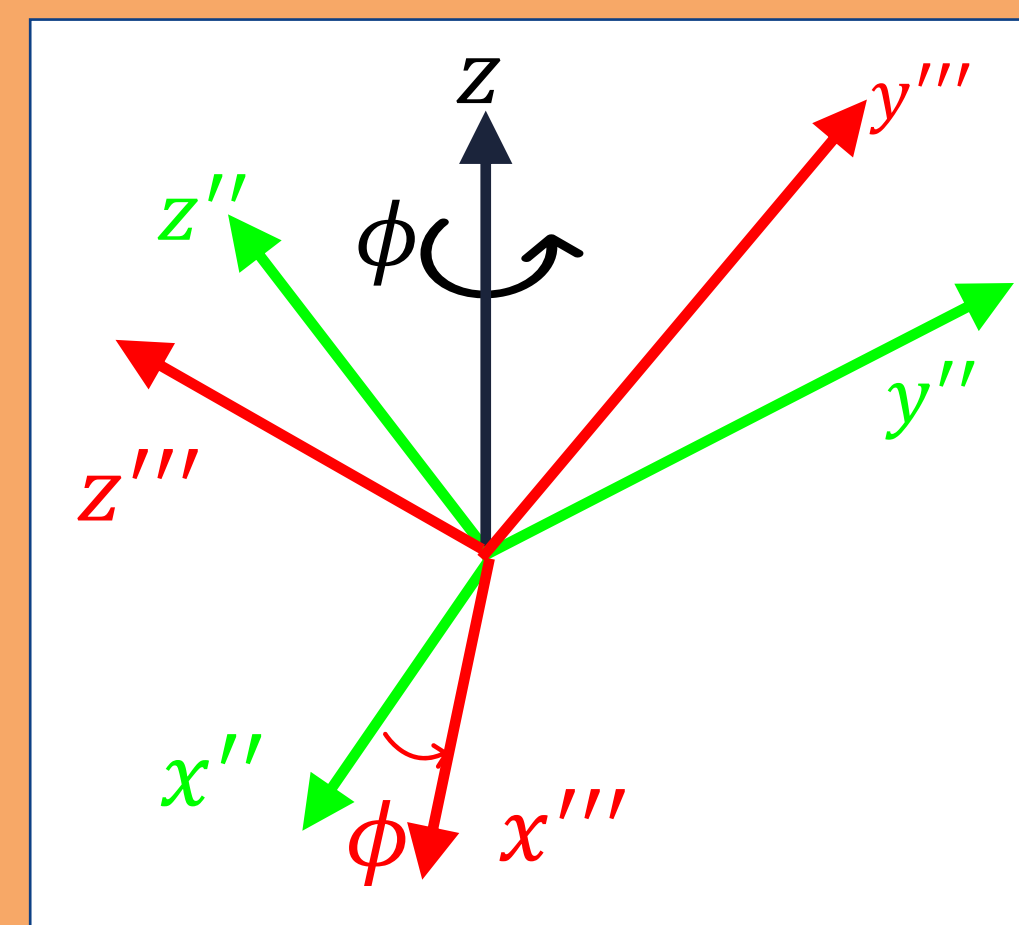


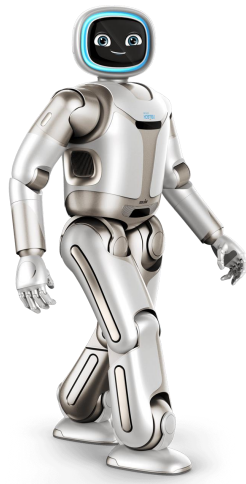
$C_1 R_Y(\theta) C_1^T$ with

$$R_Y(\theta) = \begin{bmatrix} \cos \theta & 0 & \sin \theta \\ 0 & 1 & 0 \\ -\sin \theta & 0 & \cos \theta \end{bmatrix}$$

3

YAW





Basic Definitions

Roll-Pitch-Yaw angles (fixed XYZ)

- **direct problem:** given ϕ, θ, ψ , find R

$$\begin{aligned} R_{RPY}(\psi, \theta, \phi) &= R_Z(\phi)R_Y(\theta)R_X(\psi) \Leftarrow \text{note the order of products!} \\ &\xrightarrow{\text{order of definition}} = \begin{bmatrix} c\phi c\theta & c\phi s\theta s\psi - s\phi c\psi & c\phi s\theta c\psi + s\phi s\psi \\ s\phi c\theta & s\phi s\theta s\psi + c\phi c\psi & s\phi s\theta c\psi - c\phi s\psi \\ -s\theta & c\theta s\psi & c\theta c\psi \end{bmatrix} \end{aligned}$$

- **inverse problem:** given $R = \{r_{ij}\}$, find ϕ, θ, ψ

- $r_{32}^2 + r_{33}^2 = c^2\theta, r_{31} = -s\theta \Rightarrow$

$$\theta = \text{atan2} \left\{ -r_{31}, \pm \sqrt{r_{32}^2 + r_{33}^2} \right\}$$

for $r_{31} < 0$, two symmetric values w.r.t. $\pi/2$

- if $r_{32}^2 + r_{33}^2 \neq 0$ (i.e., $c\theta \neq 0$)

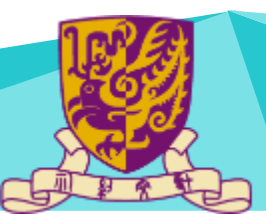
$$r_{31}/s\theta = s\psi, r_{32}/s\theta = c\psi \Rightarrow$$

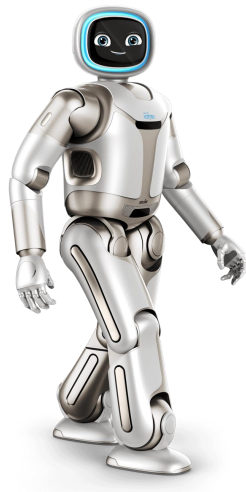
$$\psi = \text{atan2} \{ r_{32}/c\theta, r_{33}/c\theta \}$$

- similarly...

$$\phi = \text{atan2} \{ r_{21}/c\theta, -r_{11}/c\theta \}$$

- **singularities for** $\theta = \pm \pi/2 \Rightarrow$ only $\phi + \psi$ or $\phi - \psi$ are defined





Basic Definitions

... why this order in the product

$$R_{RPY}(\psi, \theta, \phi) = R_Z(\phi)R_Y(\theta)R_X(\psi)$$

order of definition

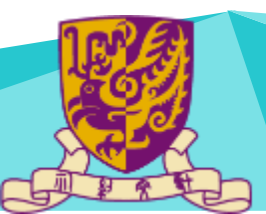
“reverse” order in the product

(pre-multiplication...)

- need to refer each rotation in the sequence to one of the original **fixed** axes
- use the angle/axis technique for each rotation in the sequence:
 $CR(\alpha)C^T$, with C being the rotation matrix **reverting** the previously made rotations (= “go back” to the original axes)

concatenating three rotations: $[[[]]]$ (post-multiplication...)

$$\begin{aligned} R_{RPY}(\psi, \theta, \phi) &= [R_X(\psi)][R_X^T(\psi)R_Y(\theta)R_X(\psi)][R_X^T(\psi)R_Y^T(\theta)R_Z(\phi)R_Y(\theta)R_X(\psi)] \\ &= R_Z(\phi)R_Y(\theta)R_X(\psi) \end{aligned}$$



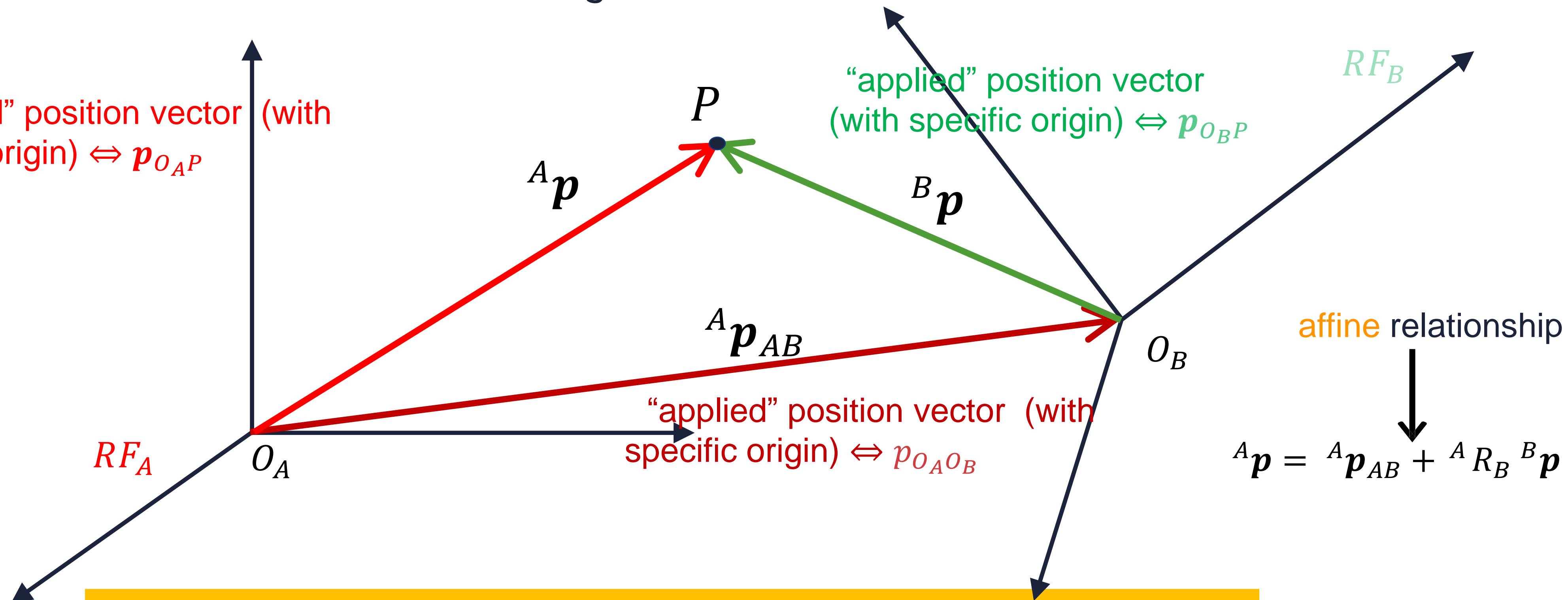


Basic Definitions

Homogeneous transformations

“applied” position vector (with specific origin) $\Leftrightarrow \mathbf{p}_{O_AP}$

“applied” position vector (with specific origin) $\Leftrightarrow \mathbf{p}_{O_BP}$



affine relationship

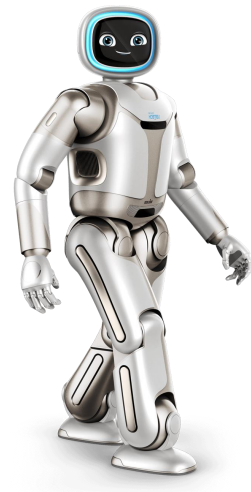
$$\mathbf{p}_A = \mathbf{p}_{AB} + \mathbf{R}_B \mathbf{p}_B$$

linear relationship

$$\mathbf{p}_{hom}^A = \begin{bmatrix} \mathbf{p}_A \\ 1 \end{bmatrix} = \begin{bmatrix} \mathbf{R}_B & \mathbf{p}_{AB} \\ \mathbf{0}^T & 1 \end{bmatrix} \begin{bmatrix} \mathbf{p}_B \\ 1 \end{bmatrix} = \mathbf{T}_B^A \mathbf{p}_{hom}^B$$

vector in homogeneous coordinates

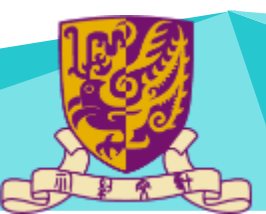
4 × 4 matrix of homogeneous transformation

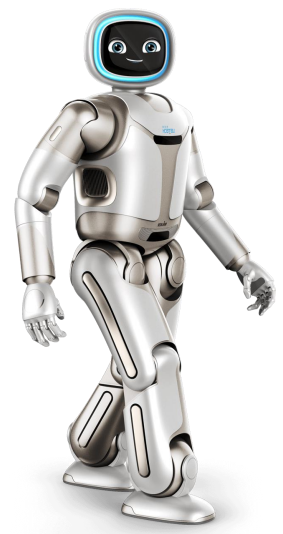


Basic Definitions

Use of homogeneous transformation T

- describes the relation between two reference frames (relative **pose** = position & orientation)
- transforms the representation of a **position** vector (applied vector starting from the **origin** of the frame) from one frame to another frame
- it is a **roto-translation** operator on vectors in the three-dimensional space
- it is always invertible $({}^A T_B)^{-1} = ({}^B T_A)$
- can be composed, i.e., ${}^A T_B {}^B T_C = {}^A T_C$ ← note: it does not commute in general!





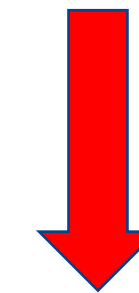
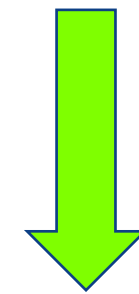
Basic Definitions

Inverse of a homogeneous transformation

exchange $A \Leftrightarrow B$

...with the original vectors/matrices...

$${}^A\mathbf{p} = {}^A\mathbf{p}_{AB} + {}^A R_B {}^B\mathbf{p} \quad {}^B\mathbf{p} = {}^B\mathbf{p}_{BA} + {}^B R_A {}^A\mathbf{p} = -{}^A R_B^T {}^A\mathbf{p}_{AB} + {}^A R_B^T {}^A\mathbf{p}$$



$$\left[\begin{array}{ccc|c} {}^A R_B & & & {}^A\mathbf{p}_{AB} \\ \hline 0 & 0 & 0 & 1 \end{array} \right]$$

${}^A T_B$

$$\left[\begin{array}{ccc|c} {}^B R_A & & & {}^B\mathbf{p}_{BA} \\ \hline 0 & 0 & 0 & 1 \end{array} \right]$$

${}^B T_A$

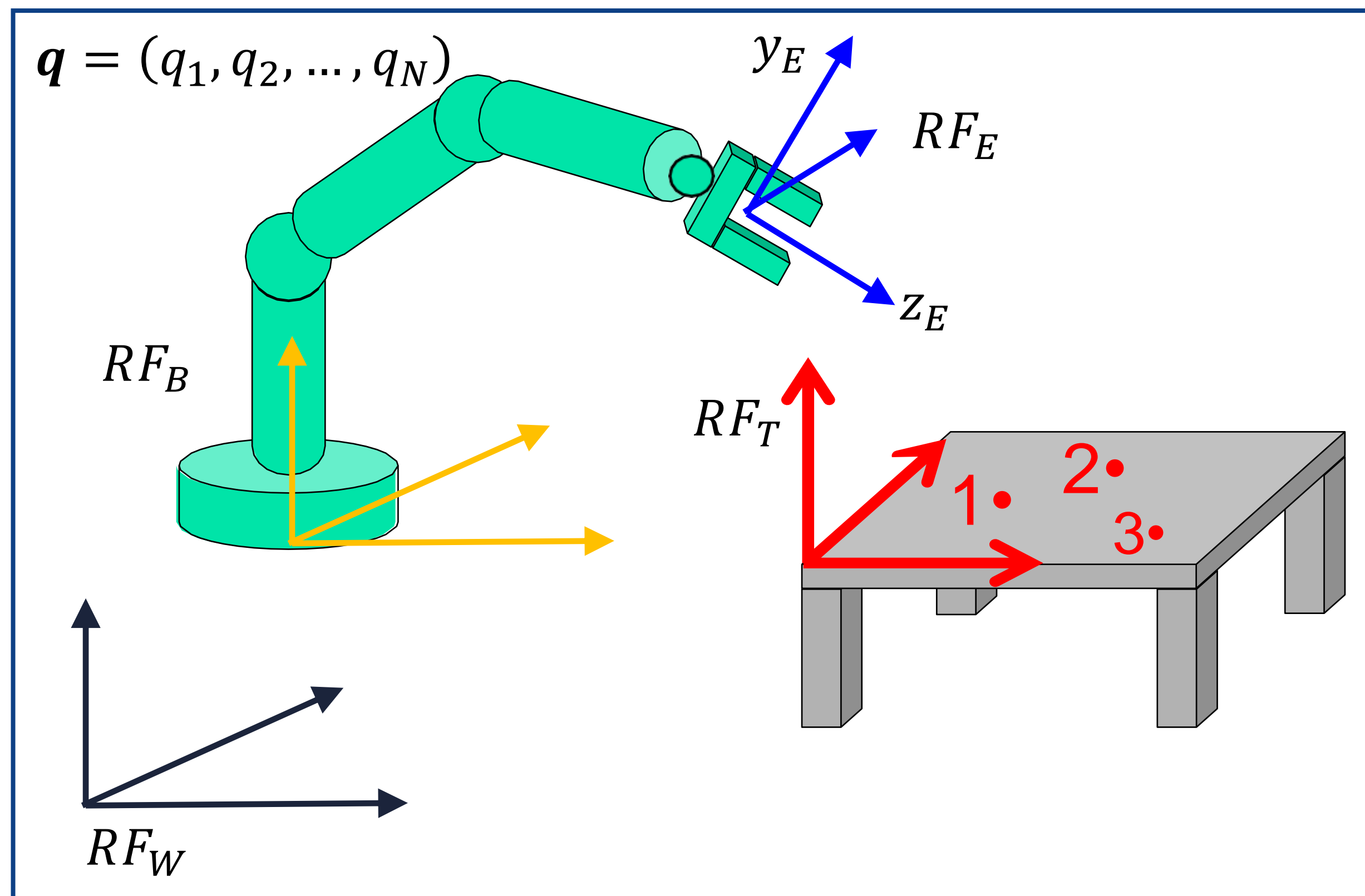
$$\left[\begin{array}{ccc|c} {}^A R_B^T & & & -{}^A R_B^T {}^A\mathbf{p}_{AB} \\ \hline 0 & 0 & 0 & 1 \end{array} \right]$$

$({}^A T_B)^{-1}$



Basic Definitions

Defining a robotic task



absolute
definition of task

task definition relative to
the robot end-effector

$${}^W T_T = {}^W T_B {}^B T_E {}^E T_T$$

known, once
the robot is
placed

direct kinematics of the
robot arm (function of q)

solve for q (inverse
kinematics)

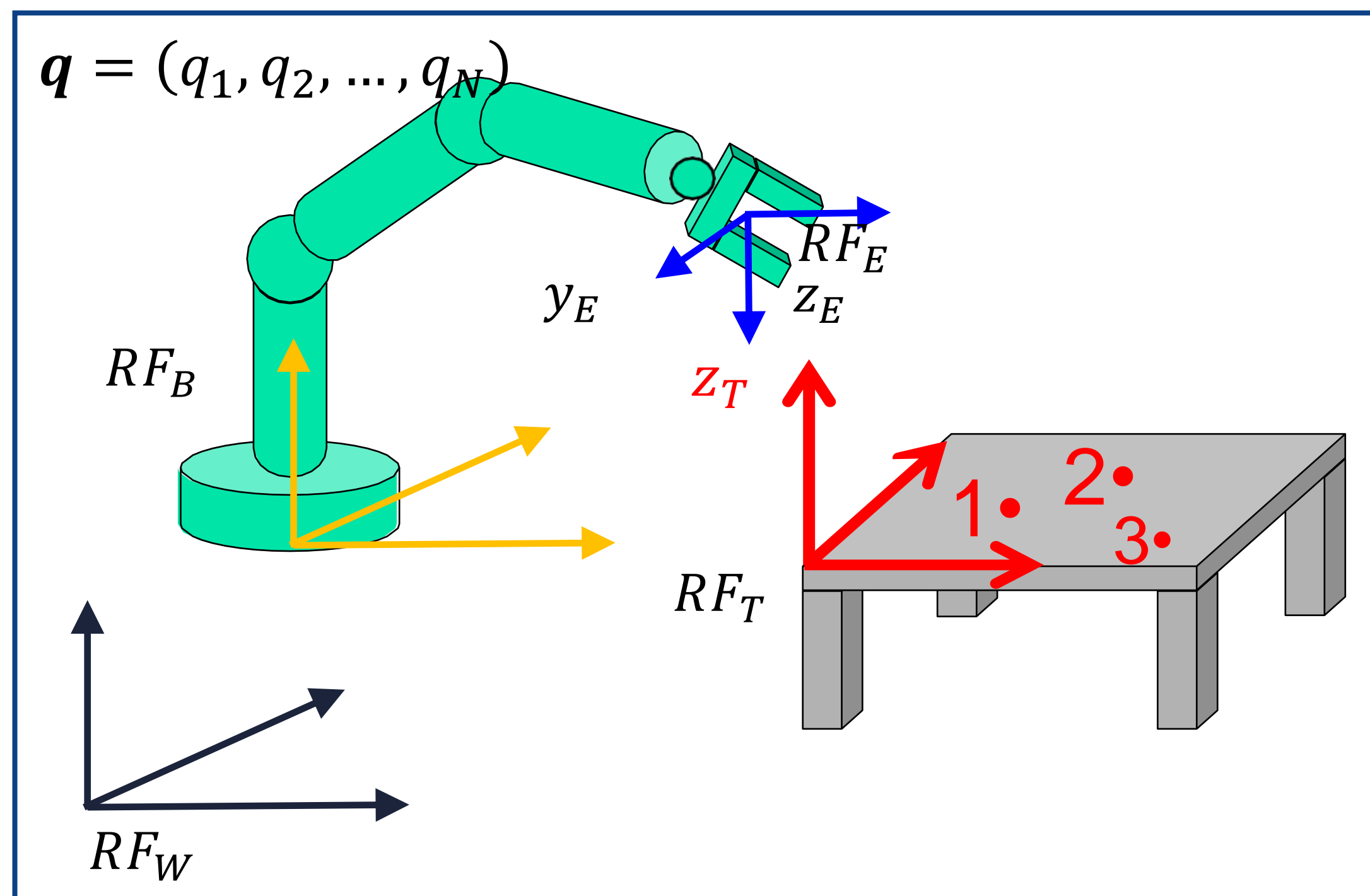
$${}^B T_E(q) = {}^W T_B^{-1} {}^W T_T {}^E T_T^{-1} = \text{constant}$$



Basic Definitions



Example of task definition



- the robot carries a **depth camera** (e.g., a Kinect) on the end-effector
- the end-effector should go to a pose above the point P on the table, pointing its approach axis z_E **downward** and being **aligned** with the table sides

$${}^E R_T = [{}^E x_T \quad {}^E y_T \quad {}^E z_T] = \begin{bmatrix} 1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & -1 \end{bmatrix}$$

- point P is known in the table frame RF_T

$${}^T \mathbf{p} = \begin{bmatrix} p_x \\ p_y \\ 0 \end{bmatrix}$$

- the robot proceeds by **centering point P** in its camera image until it senses a **depth h** from the table (in RF_E)

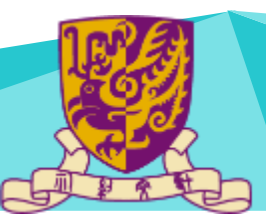
$${}^E \mathbf{p} = \begin{bmatrix} 0 \\ 0 \\ h \end{bmatrix}$$

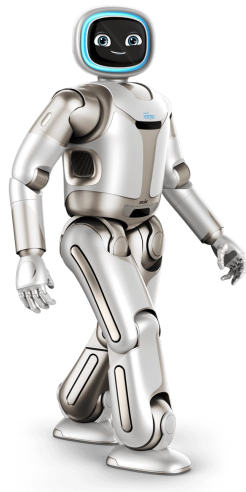
- Q: where is the EE frame w.r.t. the table frame?**

$${}^T T_E = \begin{bmatrix} {}^T R_E & {}^T \mathbf{p}_{TE} \\ 0^T & 1 \end{bmatrix} = {}^E T_T^{-1}$$

- with

$${}^T R_E = ({}^E R_T)^T = {}^E R_T \quad {}^T \mathbf{p}_{TE} = {}^T \mathbf{p} - {}^T R_E {}^E \mathbf{p} = \begin{bmatrix} p_x \\ p_y \\ h \end{bmatrix}$$





Basic Definitions

Remarks on homogeneous matrices

- the main tool used for computing the **direct kinematics** of robot manipulators
- relevant in many other applications (in robotics and beyond)
 - in positioning/orienting a vision camera (matrix bT_C with extrinsic parameters of the camera pose)
 - in computer graphics, for the real-time visualization of 3D solid objects when changing the observation point

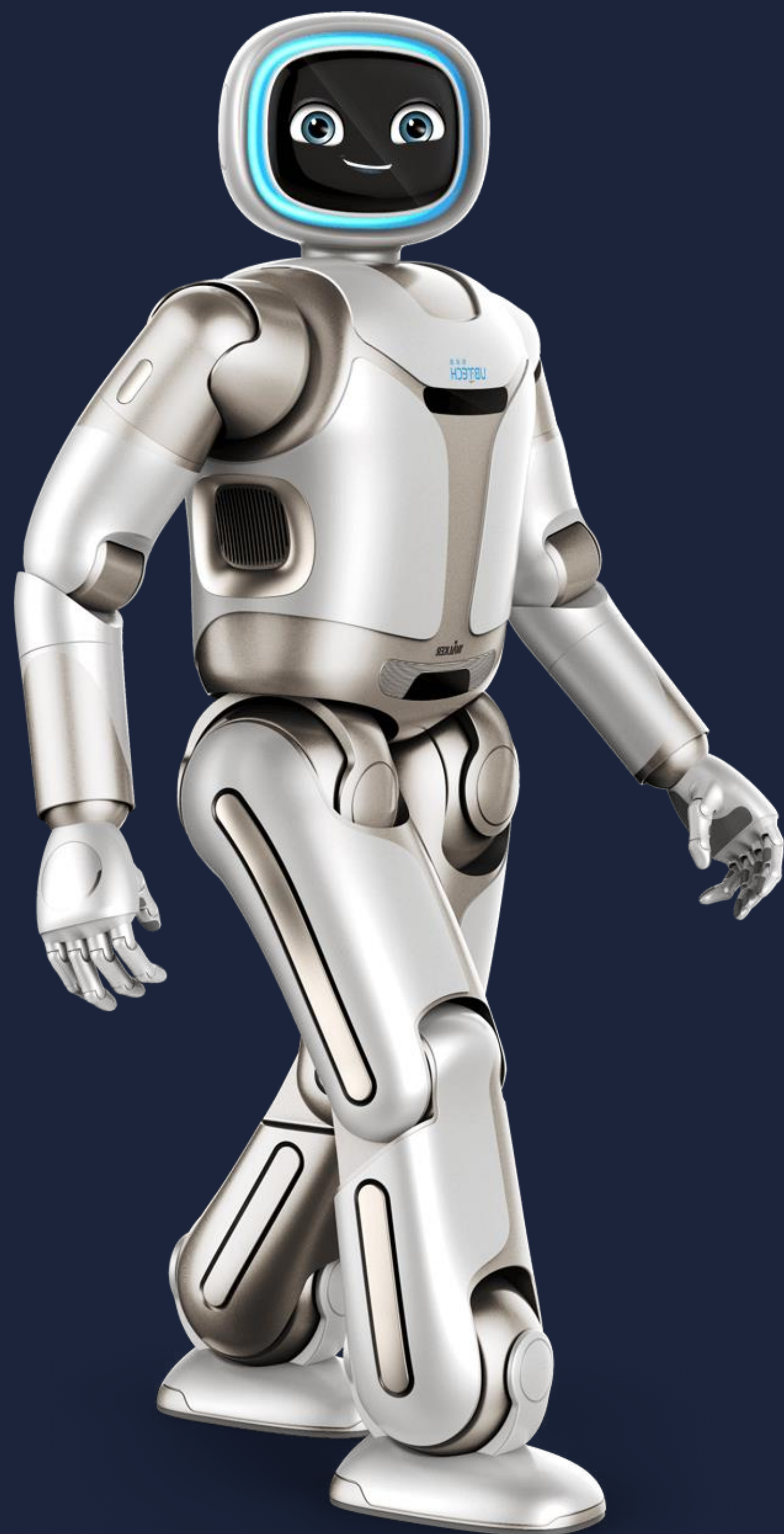
$${}^AT_B = \begin{bmatrix} {}^AR_B & {}^Ap_{AB} \\ \alpha_x & \alpha_y & \alpha_z & \sigma \end{bmatrix}$$

all zero in robotics

coefficients of perspective
deformation

scaling
coefficient

always unitary in robotics



Q&A