

THE CHINESE UNIVERSITY OF HONG KONG

DEPARTMENT OF MECHANICAL & AUTOMATION ENGINEERING

MAEG5070 Nonlinear Control Systems

Assignment #1

by

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2022-23 Term 1

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Consider the following system.

$$\dot{x}(t) = -x(t) + x^2(t), \ x(0) = x_0$$

- (a) Find the equilibrium points for the system.
- (b) Verify the solution of the system is given by

$$x(t) = \frac{x_0}{x_0 + (1 - x_0)e^t}, \ \ 0 \le t < T$$

for some T > 0.

(c) Show that $T = \ln \frac{x_0}{x_0 - 1}$ when $x_0 > 1$.

Solution:

(a)

In this nonlinear dynamical system,

$$f(x) = -x(t) + x^{2}(t) \tag{1}$$

Letting f(x) = 0 gives

$$-x(t) + x^{2}(t) = 0 \Rightarrow x^{*} = \{0, 1\}$$
 (2)

(b)

For

$$x(t) = \frac{x_0}{x_0 + (1 - x_0)e^t} \tag{3}$$

The left side of the equation is equal to

$$\dot{x}(t) = \left[\frac{x_0}{x_0 + (1 - x_0)e^t} \right]' = \frac{-x_0(1 - x_0)e^t}{[x_0 + (1 - x_0)e^t]^2} \tag{4}$$

The right side of the equation is equal to

$$-x(t) + x^{2}(t) = -\frac{x_{0}}{x_{0} + (1 - x_{0})e^{t}} + \left[\frac{x_{0}}{x_{0} + (1 - x_{0})e^{t}}\right]^{2} = \frac{-x_{0}\left[x_{0} + (1 - x_{0})e^{t}\right] + x_{0}^{2}}{\left[x_{0} + (1 - x_{0})e^{t}\right]^{2}}$$

$$= \frac{-x_{0}(1 - x_{0})e^{t}}{\left[x_{0} + (1 - x_{0})e^{t}\right]^{2}} = \text{left side}$$

$$(5)$$

Therefore, $x(t) = \frac{x_0}{x_0 + (1 - x_0)e^t}$ is the solution of the system.

(c)

Equation (3) is not defined for all $t \ge 0$. In fact, it can be seen that when $x_0 > 1$, there exists a finite t > 0 such that

$$x_0 + (1 - x_0) e^t = 0$$
 or $t = \ln \frac{x_0}{x_0 - 1}$ (6)

Therefore, Equation (3) is not defined at $t = \ln \frac{x_0}{x_0 - 1}$, which means

$$T = \ln \frac{x_0}{x_0 - 1} \tag{7}$$

It is known that the following Van del Pol equation has a limit cycle.

$$\dot{x}_1 = x_2
\dot{x}_2 = -x_1 - 0.2(x_1^2 - 1)x_2$$

Write a MATLAB program to generate $(x_1(t), x_2(t))$, $0 \le t \le 100$ for $(x_1(0), x_2(0)) = (2.3, -2)$ and $(x_1(0), x_2(0)) = (0.2, 0.3)$. Plot the phase portraits in the same Figure (that is, $x_2(t)$ vs. $x_1(t)$ for $0 \le t \le 100$). **Hint:** You can try the following Matlab 6 program

```
x01 = [2.3; -2];
x02 = [0.2; 0.3];
t0 = 0; tf = 100;
tspan=[t0 tf];
[t,x1] = ode23('limit', tspan , x01);
[t,x2] = ode23('limit', tspan , x02);
plot(x1(:,1), x1(:,2), x2(:,1), x2(:,2))
where limit is the following matlab function named as limit.m.
function xdot = limit(t,x)
xdot(1) = x(2);
xdot(2) = -x(1) -0.2*(x(1)*x(1)-1)*x(2);
xdot = xdot(:);
```

However, make sure you understand the program.

Solution:

The MATLAB code in main file is shown below:

```
clc; clf; clear all;
2 hold on;
3 \times 01 = [2.3; -2];
4 \times 02 = [0.2; 0.3];
5 \text{ t0} = 0; \text{ tf} = 100;
6 \text{ tspan} = [t0 tf];
7 [t,x1] = ode23('limit', tspan, x01);
8 [t,x2] = ode23('limit', tspan, x02);
9 plot(x1(:,1), x1(:,2),'color',[0.667 0.667 1],'LineWidth',2.5);
10 plot(x2(:,1), x2(:,2),'color',[1 0.5 0],'LineWidth',2.5);
11 xlabel('$x_1 \left(t\right)$','interpreter','latex');
12 ylabel('$x_2 \left(t\right)$','interpreter','latex');
13 legend(['$\left(x_1\left(0\right),x_2\left(0\right)\right)' ...
14
       ' =   (2.3, -2 \cdot ) , [' \cdot (x_1 \cdot (0 \cdot ), ' \dots ]
15
       'x_2\left(0\right) = \left(0.2, 0.3\right) , \dots
       'interpreter','latex');
16
17 a = get(gca,'XTickLabel');
18 set(gca,'XTickLabel',a,'FontName','Times','fontsize',12);
19 set(gcf,'renderer','painters');
20 hold off;
21 filename = "Q1_2_Code"+".pdf";
22 saveas(gcf, filename);
```

The MATLAB code in function that defines the Van del Pol equation is shown below:

```
1 function xdot = limit(t,x)
2 xdot(1) = x(2);
3 xdot(2) = -x(1) -0.2*(x(1)*x(1)-1)*x(2);
4 xdot = xdot(:);
```

And the results for phase portraits are plotted in Figure 1.

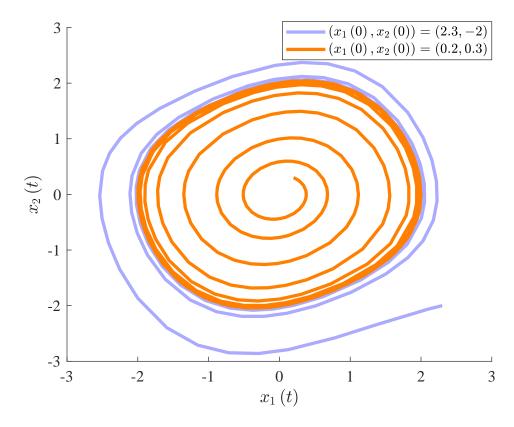


Figure 1: Phase Portraits for Given Nonlinear System.

It is known that the following system displays chaotic behavior.

$$\ddot{y} + 0.05\dot{y} + y^3 = 7.5\cos t$$

- (a) Give a state space realization for this system.
- (b) Write a MATLAB program to generate y(t), $0 \le t \le 50$ for $(y(0), \dot{y}(0)) = (3, 4)$ and $(y(0), \dot{y}(0)) = (3.01, 4.01)$. Plot them in the same Figure. (The curve should be similar to Figure 1.6, page 11 of the textbook).

Solution:

(a)

First, we need to select the state variables. Choosing the state variables as successive derivatives, we get

$$x_1 = y \tag{8a}$$

$$x_2 = \dot{y} \tag{8b}$$

Differentiating both sides and making use of Equation (8) to find \dot{x}_1 , and equation in the question to find $\tilde{y} = \dot{x}_2$, we obtain the state equations (Nise, 2020). The combined state and output equations are

$$\dot{x}_1 = x_2 \tag{9a}$$

$$\dot{x}_2 = -x_1^3 - 0.05x_2 + 7.5\cos t \tag{9b}$$

In vector-matrix form,

$$\dot{x}(t) = f(x(t), t) \tag{10}$$

where

$$x = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}, \quad f(x(t), t) = \begin{bmatrix} x_2 \\ -x_1^3 - 0.05x_2 + 7.5\cos t \end{bmatrix}$$
 (11)

(b)

The MATLAB code in main file is shown below:

```
1 clc; clf; clear all;
2 hold on;
3 x01 = [3; 4];
4 x02 = [3.01; 4.01];
5 t0 = 0; tf = 50;
6 tspan = [t0 tf];
7 [t,x1] = ode23('limit', tspan , x01);
8 plot(t,x1(:,1),'color',[0.667 0.667 1],'LineWidth',2.5);
9 [t,x2] = ode23('limit', tspan , x02);
10 plot(t,x2(:,1),'color',[1 0.5 0],'LineWidth',2.5);
11 grid on;
```

```
12 xlabel('$t$','interpreter','latex');
   ylabel('$y \left(t\right)$','interpreter','latex');
13
   legend(['$\left(0\right),\dot{y}\left(0\right)\right)' ...
14
       '=\left(3,4\right)$'],['$\left(y\left(0\right),' ...
15
       ' \det{y} \left(0 \right) = \left(3.01, 4.01 \right) , ...
16
17
       'interpreter','latex');
   a = get(gca,'XTickLabel');
18
   set (gca,'XTickLabel',a,'FontName','Times','fontsize',12);
19
  set (gcf,'renderer','painters');
20
21 hold off;
22 filename = "Q1_3_Code"+".pdf";
23 saveas(gcf, filename);
```

The MATLAB code in function that defines the Van del Pol equation is shown below:

```
1 function xdot = limit(t,x)
2 xdot(1) = x(2);
3 xdot(2) = -x(1)*x(1)*x(1)-0.05*x(2)+7.5*cos(t);
4 xdot = xdot(:);
```

And the results for y(t) are plotted in Figure 2.

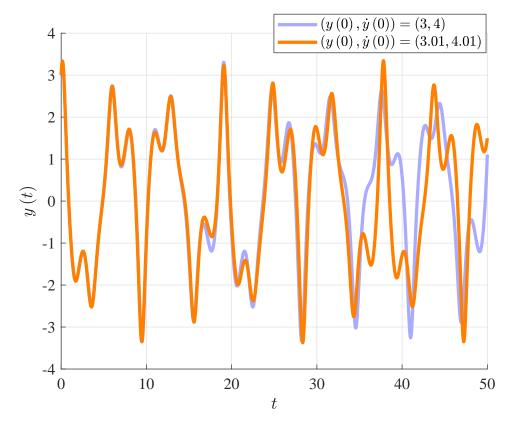


Figure 2: Results for Chaotic Behavior with Different Initial Conditions.

References

Nise, N. S. (2020). Control systems engineering. John Wiley & Sons.



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MAEG5070 Nonlinear Control Systems

Assignment #2

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For each of the following systems, find all equilibrium points and determine the type of each isolated equilibrium.

(a)

$$\dot{x}_1 = x_2
\dot{x}_2 = -x_1 + \frac{x_1^3}{4} - x_2$$

(b)

$$\dot{x}_1 = -2x_1 + x_2(1+x_1)
\dot{x}_2 = -x_1(1+x_1)$$

Solution:

(a)

The equilibrium points $x^* = \begin{bmatrix} x_1^* \\ x_2^* \end{bmatrix}$ satisfy

$$\begin{cases} x_2^* = 0 \\ -x_1^* + \frac{x_1^{*3}}{4} - x_2^* = 0 \end{cases} \Rightarrow x^* = \left\{ \begin{bmatrix} 0 \\ 0 \end{bmatrix}, \begin{bmatrix} 2 \\ 0 \end{bmatrix}, \begin{bmatrix} -2 \\ 0 \end{bmatrix} \right\}$$
 (1)

Taking the Jacobian of the appropriate function yields that

$$\frac{\partial f}{\partial x} = \begin{bmatrix} 0 & 1\\ -1 + \frac{3}{4}x_1^2 & -1 \end{bmatrix} \tag{2}$$

For
$$x^* = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$
,

$$A_{x^*} = \frac{\partial f}{\partial x}\Big|_{x=x^*} = \begin{bmatrix} 0 & 1\\ -1 & -1 \end{bmatrix}$$
 (3)

The eigenvalues of A_{x^*} are

$$\lambda_{1,2} = \frac{-1 \pm \sqrt{3}i}{2} \tag{4}$$

Therefore, the equilibrium point (0,0) is a stable focus.

For
$$x^* = \begin{bmatrix} 2 \\ 0 \end{bmatrix}$$
,

$$A_{x^*} = \left. \frac{\partial f}{\partial x} \right|_{x=x^*} = \begin{bmatrix} 0 & 1\\ 2 & -1 \end{bmatrix} \tag{5}$$

The eigenvalues of A_{x^*} are

$$\lambda_{1,2} = \begin{bmatrix} 1 \\ -2 \end{bmatrix} \tag{6}$$

Therefore, the equilibrium point (2,0) is a saddle point.

For
$$x^* = \begin{bmatrix} -2 \\ 0 \end{bmatrix}$$
,

$$A_{x^*} = \left. \frac{\partial f}{\partial x} \right|_{x=x^*} = \begin{bmatrix} 0 & 1\\ 2 & -1 \end{bmatrix} \tag{7}$$

The eigenvalues of A_{x^*} are

$$\lambda_{1,2} = \begin{bmatrix} 1 \\ -2 \end{bmatrix} \tag{8}$$

Therefore, the equilibrium point (-2,0) is a saddle point.

(b)

The equilibrium points $x^* = \begin{bmatrix} x_1^* \\ x_2^* \end{bmatrix}$ satisfy

$$\begin{cases} -2x_1^* + x_2^* \left(1 + x_1^* \right) = 0 \\ -x_1^* \left(1 + x_1^* \right) = 0 \end{cases} \Rightarrow x^* = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$
 (9)

Taking the Jacobian of the appropriate function yields that

$$\frac{\partial f}{\partial x} = \begin{bmatrix} -2 + x_2 & 1 + x_1 \\ -1 + 2x_1 & 0 \end{bmatrix} \tag{10}$$

For
$$x^* = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$
,

$$A_{x^*} = \left. \frac{\partial f}{\partial x} \right|_{x=x^*} = \begin{bmatrix} -2 & 1\\ -1 & 0 \end{bmatrix} \tag{11}$$

The eigenvalues of A_{x^*} are

$$\lambda_{1,2} = \begin{bmatrix} -1 \\ -1 \end{bmatrix} \tag{12}$$

Therefore, the equilibrium point (0,0) is a stable node.

Consider the nonlinear system

$$\dot{x}_1 = x_2 - x_1(x_1^2 + x_2^2 - 1)^2, x_1(0) = x_{10}$$

 $\dot{x}_2 = -x_1 - x_2(x_1^2 + x_2^2 - 1)^2, x_2(0) = x_{20}$

- (a) Show that the system has a limit cycle.
- (b) Determine the stability of the limit cycle.

(*Hint:*) Use polar coordinates.

Solution:

(a)

The polar coordinates are introduced as follows:

$$r = \left(x_1^2 + x_2^2\right)^{1/2} \tag{13}$$

and

$$\theta = \tan^{-1}(x_2/x_1) \tag{14}$$

Rearranging Equation (13) gives

$$r^2 = x_1^2 + x_2^2 \tag{15}$$

Taking the derivative of Equation (15) yields

$$2r\frac{dr}{dt} = 2x_1 \frac{dx_1}{dt} + 2x_2 \frac{dx_2}{dt}$$
 (16)

Substituting the conditions in the question into Equation (16) gets

$$2r\frac{dr}{dt} = 2x_1 \left[x_2 - x_1 \left(x_1^2 + x_2^2 - 1 \right)^2 \right] + 2x_2 \left[-x_1 - x_2 \left(x_1^2 + x_2^2 - 1 \right)^2 \right]$$
 (17)

Simplifying Equation (17) leads to

$$\frac{dr}{dt} = -r\left(r^2 - 1\right)^2\tag{18}$$

Rearranging Equation (14) gives

$$\tan \theta = \frac{x_2}{x_1} \tag{19}$$

Differentiating Equation (19) yields

$$\frac{1}{\cos^2 \theta} \frac{d\theta}{dt} = \frac{1}{x_1} \frac{dx_2}{dt} - x_2 \frac{1}{x_1^2} \frac{dx_1}{dt}$$
 (20)

Substituting the conditions in the question into Equation (20) gets

$$\frac{1}{\cos^2 \theta} \frac{d\theta}{dt} = \frac{1}{x_1} \left[-x_1 - x_2 \left(x_1^2 + x_2^2 - 1 \right)^2 \right] - x_2 \frac{1}{x_1^2} \left[x_2 - x_1 \left(x_1^2 + x_2^2 - 1 \right)^2 \right]$$
(21)

Simplifying Equation (21) leads to

$$\frac{d\theta}{dt} = -1\tag{22}$$

When the state starts on the unit circle, the above equation shows that $\dot{r}(t) = 0$. Therefore, the state will circle around the origin with a period $1/2\pi$. When r > 1, then $\dot{r} < 0$. This implies that the state tends toward the unit circle from the outside. When r < 1, then $\dot{r} < 0$. This implies that the state tends to diverge from it. Therefore, the unit circle is a semi-stable limit cycle (Slotine et al., 1991).

(b)

When the state starts on the unit circle, the above equation shows that $\dot{r}(t) = 0$. Therefore, the state will circle around the origin with a period $1/2\pi$. When r > 1, then $\dot{r} < 0$. This implies that the state tends toward the unit circle from the outside. When r < 1, then $\dot{r} < 0$. This implies that the state tends to diverge from it. Therefore, the limit cycle is semi-stable.

Consider the system

$$\dot{x}_1 = x_2
 \dot{x}_2 = ax_1 + bx_2 - x_1^2 x_2 - x_1^3$$

Show that there can be no limit cycle if b < 0.

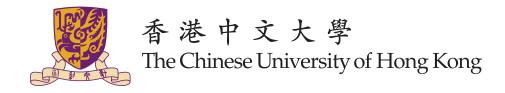
Solution:

$$\frac{\partial f_1}{\partial x_1} + \frac{\partial f_2}{\partial x_2} = b - x_1^2 < 0 \tag{23}$$

By Bendixson's criterion, there are no periodic orbits. Therefore, there can be no limit cycle if b < 0.

References

Slotine, J.-J. E., Li, W., et al. (1991). Applied nonlinear control, volume 199. Prentice hall Englewood Cliffs, NJ.



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MAEG5070 Nonlinear Control Systems

Assignment #3

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2022-23 Term 1

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Does the system have any limit cycle?

$$\dot{x}_1 = 2x_2^2 \sin x_2
\dot{x}_2 = 1 - \cos x_1 + 2x_2$$

Solution:

$$\frac{\partial f_1}{\partial x_1} + \frac{\partial f_2}{\partial x_2} = 2 > 0 \tag{1}$$

By Bendixson's criterion, there are no periodic orbits. Therefore, there can be no limit cycle.

Consider the following nonlinear equation.

$$\dot{x}_1 = x_2 - x_1^2 + 3x_2^3
\dot{x}_2 = x_3 - 2x_2x_1 - x_1x_3
\dot{x}_3 = 3x_1 + 2x_3x_2 - 2x_3 + u$$

- (a) Find the Jacobian linearization of the system at the origin.
- (b) Using the Lyapunov's linearization method to determine the stability property of the closed-loop system under the state feedback control law u = -Kx for K = [-4 3 1].

Solution:

(a)

The Jacobian matrix of the nonlinear equation is (Close et al., 2001)

$$\frac{\partial f(x,u)}{\partial x} = \begin{bmatrix}
\frac{\partial f_1(x)}{\partial x_1} & \frac{\partial f_1(x)}{\partial x_2} & \frac{\partial f_1(x)}{\partial x_3} \\
\frac{\partial f_2(x)}{\partial x_1} & \frac{\partial f_2(x)}{\partial x_2} & \frac{\partial f_2(x)}{\partial x_3} \\
\frac{\partial f_3(x)}{\partial x_1} & \frac{\partial f_3(x)}{\partial x_2} & \frac{\partial f_3(x)}{\partial x_3}
\end{bmatrix} = \begin{bmatrix}
-2x_1 & 9x_2^2 + 1 & 0 \\
-2x_2 - x_3 & -2x_1 & -x_1 + 1 \\
3 & 2x_3 & 2x_2 - 2
\end{bmatrix}$$
(2)

For the system at the origin,

$$A = \frac{\partial f(x, u)}{\partial x} \Big|_{x=0, u=0} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 3 & 0 & -2 \end{bmatrix}$$
 (3)

$$B = \frac{\partial f(x, u)}{\partial u} \Big|_{x=0, u=0} = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$
 (4)

Therefore, the Jacobian linearization of the system at the origin is

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 3 & 0 & -2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} u \tag{5}$$

(b)

$$A - BK = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 3 & 0 & -2 \end{bmatrix} - \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \begin{bmatrix} -4 & -3 & -1 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 7 & 3 & -1 \end{bmatrix}$$
 (6)

The eigenvalues of A - BK are

$$\lambda_1 = -1.5370 + 1.0064i$$

$$\lambda_2 = -1.5370 - 1.0064i$$

$$\lambda_3 = 2.0739$$
(7)

Because the real part of one of the eigenvalues of $A - BK - \lambda_3$ —is positive, the closed-loop system under the state feedback control law u = -Kx for $K = \begin{bmatrix} -4 & -3 & -1 \end{bmatrix}$ is unstable.

The motion of the ball and beam system can be described by

$$\begin{array}{rcl} \dot{x}_1(t) & = & x_2(t) \\ \dot{x}_2(t) & = & Bx_1(t)x_4^2(t) - BGsin(x_3(t)) \\ \dot{x}_3(t) & = & x_4(t) \\ \dot{x}_4(t) & = & u(t) \\ y(t) & = & x_1(t) \end{array}$$

where x_1 is the position of the ball, u is the torque applied to the beam, $G = 9.81 \ m/s^2$ is the acceleration of gravity, and B = 0.7134 is a constant.

(a) Show that the Jacobian linearization of (1) at the origin is given by

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & -BG & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \end{bmatrix} u = Ax + bu$$

- (b) Verify that the pair (A, b) is controllable, i.e., the matrix $[b \ Ab \ \cdots \ A^{n-1}b]$ is nonsingular.
- (c) Using Arkerman's Formula to find K so that the eigenvalues of A bK are $\{-1, -2, -3, -24\}$.
- (d) Simulate the closed-loop system composed of (1) and u = -Kx with $x(0) = \alpha[1, 1, 1, 1]$ for $\alpha = 1, 20$ from t = 0 to t = 20. Is the equilibrium point x = 0 of the closed-loop system globally asymptotically stable?

Arkerman's Formula

Let $A \in \mathbb{R}^{n \times n}$ and $b \in \mathbb{R}^n$. Assume the pair (A, b) is controllable, i.e., the matrix $[b \ Ab \ \cdots \ A^{n-1}b]$ is nonsingular. Let $q(s) = s^n + \alpha_1 s^{n-1} + \cdots + \alpha_{n-1} s + \alpha_n$ which is called the desired polynomial. Let $q(F) = F^n + \alpha_1 F^{n-1} + \cdots + \alpha_{n-1} F + \alpha_n I_n$

$$K = \left[\begin{array}{cccc} 0 & \cdots & 0 & 1 \end{array} \right]_{1\times n} [b \ Ab \ \cdots \ A^{n-1}b]^{-1}q(F)$$

is such that

$$\det(sI - (A - BK)) = q(s)$$

Solution:

(a)

The Jacobian matrix of the nonlinear equation is

$$\frac{\partial f\left(x,u\right)}{\partial x} = \begin{bmatrix}
\frac{\partial f_{1}(x)}{\partial x_{1}} & \frac{\partial f_{1}(x)}{\partial x_{2}} & \frac{\partial f_{1}(x)}{\partial x_{3}} & \frac{\partial f_{1}(x)}{\partial x_{4}} \\
\frac{\partial f_{2}(x)}{\partial x_{1}} & \frac{\partial f_{2}(x)}{\partial x_{2}} & \frac{\partial f_{2}(x)}{\partial x_{3}} & \frac{\partial f_{2}(x)}{\partial x_{4}} \\
\frac{\partial f_{3}(x)}{\partial x_{1}} & \frac{\partial f_{3}(x)}{\partial x_{2}} & \frac{\partial f_{3}(x)}{\partial x_{3}} & \frac{\partial f_{3}(x)}{\partial x_{4}} \\
\frac{\partial f_{4}(x)}{\partial x_{1}} & \frac{\partial f_{4}(x)}{\partial x_{2}} & \frac{\partial f_{4}(x)}{\partial x_{3}} & \frac{\partial f_{4}(x)}{\partial x_{4}}
\end{bmatrix} = \begin{bmatrix}
0 & 1 & 0 & 0 \\
Bx_{4}^{2}(t) & 0 & -BG\cos(x_{3}(t)) & 2Bx_{1}(t)x_{4}(t) \\
0 & 0 & 0 & 1 \\
0 & 0 & 0 & 0
\end{bmatrix}$$
(8)

For the system at the origin,

$$A = \frac{\partial f(x, u)}{\partial x}\Big|_{x=0, u=0} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & -BG & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$
(9)

$$B = \frac{\partial f(x, u)}{\partial u}\Big|_{x=0, u=0} = \begin{bmatrix} 0\\0\\0\\1 \end{bmatrix}$$
 (10)

Therefore, the Jacobian linearization of the system at the origin is

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & -BG & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \end{bmatrix} u \tag{11}$$

(b)

$$\begin{bmatrix} B & AB & A^2B & A^3B \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 & -BG \\ 0 & 0 & -BG & 0 \\ 0 & 1 & 0 & 0 \\ 1 & 0 & 0 & 0 \end{bmatrix}$$
(12)

$$\operatorname{rank} \begin{bmatrix} B & AB & A^2B & A^3B \end{bmatrix} = 4 \tag{13}$$

Therefore, the matrix $\begin{bmatrix} B & AB & A^2B & A^3B \end{bmatrix}$ is nonsingular, which indicates that the pair (A, b) is controllable.

(c)

According to Arkerman's Formula,

$$K = \begin{bmatrix} 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 & 0 & 0 & -BG \\ 0 & 0 & -BG & 0 \\ 0 & 1 & 0 & 0 \\ 1 & 0 & 0 & 0 \end{bmatrix}^{-1} q(A)$$
(14)

Because the eigenvalues of A - bK are $\{-1, -2, -3, -24\}$ and $\det(sI - (A - BK)) = q(s)$, the desired polynomial is

$$q(s) = (s+1)(s+2)(s+3)(s+24)$$
(15)

Therefore,

$$q(A) = (A+I) \cdot (A+2I) \cdot (A+3I) \cdot (A+24I)$$

$$= \begin{bmatrix} 144 & 270 & 1084.8 & -210 \\ 0 & 144 & -1889.6 & -1084.8 \\ 0 & 0 & 144 & 270 \\ 0 & 0 & 0 & 144 \end{bmatrix}$$
(16)

where *I* is the identity matrix. Then, we can get

$$K = \begin{bmatrix} 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 & 0 & 0 & -6.9985 \\ 0 & 0 & -6.9985 & 0 \\ 0 & 1 & 0 & 0 \\ 1 & 0 & 0 & 0 \end{bmatrix}^{-1} \begin{bmatrix} 144 & 270 & 1084.8 & -210 \\ 0 & 144 & -1889.6 & -1084.8 \\ 0 & 0 & 144 & 270 \\ 0 & 0 & 0 & 144 \end{bmatrix}$$
(17)
$$= \begin{bmatrix} -20.5760 & -38.5799 & 155.0000 & 30.0000 \end{bmatrix}$$

Instead of Arkerman's Formula, I also use another way to find out the answer, whose MATLAB codes are shown below:

```
1 clc; clear all;
2 B = 0.7134;
3 G = 9.81;
4 BG = B*G;
5 syms k1 k2 k3 k4
6 sp = sym('sp', [4 \ 4 \ 4]);
7 lambda = [-1 -2 -3 -24];
8 \text{ detsp} = \text{sym}('\text{detsp'}, [1 \ 4]);
9 for i = 1:4
10
        sp(:,:,i) = [-lambda(i) 1 0 0;
           0 -lambda(i) -BG 0;
11
12
           0 0 -lambda(i) 1;
13
            -k1 - k2 - k3 - k4 - lambda(i);
14
       detsp(i) = det(sp(:,:,i));
15 end
16
   [k1, k2, k3, k4] = solve(detsp==0);
```

(d)

I use the Simulink model as shown in Figure 1 to simulate the closed-loop system composed of (1) and u = -Kx with $x(0) = \alpha \begin{bmatrix} 1 & 1 & 1 \end{bmatrix}$ for $\alpha = 1$ and 20 from t = 0 to t = 20 s.

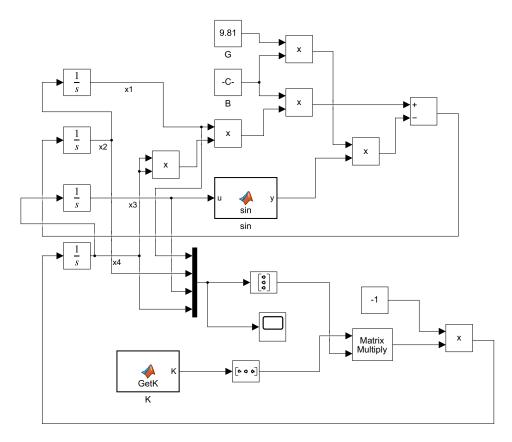


Figure 1: Simulink model to simulate the closed-loop system composed of (1) and u = -Kx with $x(0) = \alpha \begin{bmatrix} 1 & 1 & 1 \end{bmatrix}$ for $\alpha = 1$ and 20 from t = 0 to t = 20 s.

The results I get from the simulation is shown in Figure 2 and 3 for $\alpha = 1$ and 20, respectively, From Figure 3, we can know that for the initial conditions of $x(0) = 20\begin{bmatrix} 1 & 1 & 1 & 1 \end{bmatrix}$, the system is unstable. Therefore, the equilibrium point x = 0 of the closed-loop system is not globally asymptotically stable.

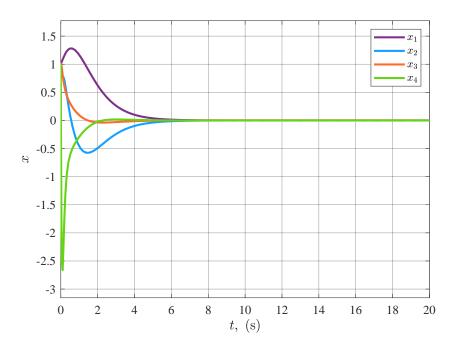


Figure 2: Simulation results for the system with $\alpha = 1$.

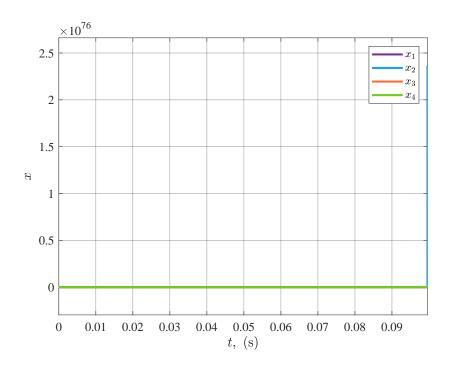
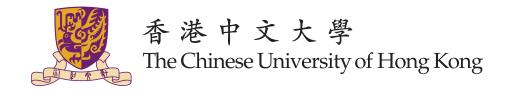


Figure 3: Simulation results for the system with $\alpha = 20$.

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THE CHINESE UNIVERSITY OF HONG KONG

DEPARTMENT OF MECHANICAL & AUTOMATION ENGINEERING

MAEG5070 Nonlinear Control Systems

Assignment #4

by

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2022-23 Term 1

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For the following systems, find the equilibrium points and determine their stability. Indicate whether the stability is asymptotic, and whether it is global.

$$\dot{x} = -x^3 + \sin^4 x \tag{1}$$

(b)
$$\dot{x} = (5 - x)^5 \tag{2}$$

Solution:

(a) The equilibrium points x^* satisfy $-x^{*3} + \sin^4 x^* = 0$. Obviously, $x^* = 0$ is one solution. Next, I will prove that $x^* = 0$ is the only solution. Let $f(x) = -x^3 + \sin^4 x$.

$$f'(x) = 4\sin^3 x \cos x - 3x^2 \tag{3}$$

Because $\sin x \cos x \le \frac{\sin^2 x + \cos^2 x}{2} = \frac{1}{2}$ (Cauchy–Schwarz inequality),

$$f'(x) = 4\sin^2 x \sin x \cos x - 3x^2 \le 2\sin^2 x - 3x^2 \le 2x^2 - 3x^2 = -x^2 \le 0$$
 (4)

Hence, f(x) is a monotonically decreasing function, which indicates that $x^* = 0$ is the only solution. Therefore, the equilibrium point for this system is $x^* = 0$. Then, the following Lyapunov function is selected as the candidate:

$$V\left(x\right) = \frac{1}{2}x^2\tag{5}$$

V(x) is positive definite for $\forall x \in \mathbf{R} - \{0\}$. Taking the derivative of Equation (5) yields that

$$\dot{V}(x) = x\dot{x} = x\left(-x^3 + \sin^4 x\right) \tag{6}$$

From the analysis above for f(x), it can be concluded that f(x) > 0 when x < 0 and f(x) < 0 when x > 0. Combing this conclusion with Equation (6) obtains $\dot{V}(x) < 0$ for $\forall x \in \mathbf{R} - \{0\}$, indicating that $\dot{V}(x)$ is negative definite. Therefore, the system is globally asymptotically stable.

(b) The equilibrium points x^* satisfy $(5 - x^*)^5 = 0$. Obviously, $x^* = 5$ is one solution and $(5 - x)^5$ is monotonically-decreasing. Therefore, the equilibrium point for this system is $x^* = 5$. Then, the following Lyapunov function is selected as the candidate:

$$V(x) = \frac{1}{2} (5 - x)^2 \tag{7}$$

V(x) is positive definite for $\forall x \in \mathbf{R} - \{5\}$. Taking the derivative of Equation (7) yields that

$$\dot{V}(x) = -(5-x)\dot{x} = -(5-x)^6 < 0 \text{ for } \forall x \in \mathbf{R} - \{5\}$$
 (8)

Therefore, $\dot{V}(x)$ is negative definite, which means that the system is globally asymptotically stable.

Consider the following pendulum equation:

$$\dot{x}_1 = x_2
\dot{x}_2 = -a_1 \sin x_1 - a_2 x_2$$
(9)

where $a_1 > 0$ and $a_2 > 0$.

- (a) Show the equilibrium point x = 0 is stable using the Lyapunov function candidate $V(x) = a_1 (1 \cos x_1) + \frac{1}{2} x_2^2$. Can you conclude the asymptotic stability of the equilibrium point x = 0 with this V(x)?
- (b) Consider the Lyapunov function candidate

$$V(x) = \frac{1}{2} \left(p_{11} x_1^2 + 2p_{12} x_1 x_2 + p_{22} x_2^2 \right) + a_1 \left(1 - \cos x_1 \right)$$
 (10)

where $p_{22} = 1$ and $p_{11} = a_2 p_{12}$. Can you find appropriate value for p_{12} to conclude the asymptotic stability of the equilibrium point x = 0 with this V(x)?

Solution:

(a)
$$V(x) = a_1 (1 - \cos x_1) + \frac{1}{2} x_2^2 > a_1 (1 - \cos x_1) \ge a_1 (1 - 1) = 0$$
 (11)

$$\dot{V}(x) = a_1 \sin x_1 \dot{x}_1 + x_2 \dot{x}_2 = a_1 x_2 \sin x_1 + x_2 \left(-a_1 \sin x_1 - a_2 x_2 \right) = -a_2 x_2^2 \le 0$$
 (12)

Therefore, V(x) is positive definite, and $\dot{V}(x)$ is negative semi-definite, which means I can not conclude the asymptotic stability of the equilibrium point x = 0 with this V(x).

(b)

$$V(x) = \frac{1}{2} \left(p_{11} x_1^2 + 2p_{12} x_1 x_2 + p_{22} x_2^2 \right) + a_1 \left(1 - \cos x_1 \right)$$

$$= \frac{1}{2} \left(a_2 p_{12} x_1^2 + 2p_{12} x_1 x_2 + x_2^2 \right) + a_1 \left(1 - \cos x_1 \right)$$

$$> a_1 \left(1 - \cos x_1 \right) \ge a_1 \left(1 - 1 \right) = 0$$

$$(13)$$

$$\dot{V}(x) = p_{11}x_1\dot{x}_1 + p_{12}\dot{x}_1x_2 + p_{12}x_1\dot{x}_2 + p_{22}x_2\dot{x}_2 + a_1\sin x_1\dot{x}_1
= p_{11}x_1x_2 + p_{12}x_2^2 + p_{12}x_1(-a_1\sin x_1 - a_2x_2)
+ p_{22}x_2(-a_1\sin x_1 - a_2x_2) + a_1x_2\sin x_1
= a_2p_{12}x_1x_2 + p_{12}x_2^2 + p_{12}x_1(-a_1\sin x_1 - a_2x_2)
+ x_2(-a_1\sin x_1 - a_2x_2) + a_1x_2\sin x_1
= (p_{12} - a_2)x_2^2 - a_1p_{12}x_1\sin x_1$$
(14)

For $x_1 \in (-\pi, \pi)$ and $x_2 \in \mathbf{R}$, $0 < p_{12} < a_2$ is selected to make $\dot{V}(x)$ ND. Therefore, the appropriate value for p_{12} , i.e. $0 < p_{12} < a_2$, can be selected to conclude that the equilibrium point x = 0 is locally asymptotic stable.

However, I can not find appropriate value for p_{12} to conclude the globally asymptotic stability of the equilibrium point x = 0 with this V(x). Because for $\forall p_{12} \in \mathbf{R}^+, \exists k \in \mathbf{Z}$, which satisfies

$$k > -\frac{(p_{12} - a_2)x_2^2}{2\pi a_1 p_{12}} - \frac{3}{4}$$
 (15)

so that when $x_1 = 2k\pi + \frac{3}{2}\pi$,

$$\dot{V}(x) = (p_{12} - a_2) x_2^2 - a_1 p_{12} x_1 \sin x_1
= (p_{12} - a_2) x_2^2 + a_1 p_{12} x_1
= (p_{12} - a_2) x_2^2 + a_1 p_{12} \left(2k\pi + \frac{3}{2}\pi \right)
> (p_{12} - a_2) x_2^2 + a_1 p_{12} \left[2\pi \left(-\frac{(p_{12} - a_2) x_2^2}{2\pi a_1 p_{12}} - \frac{3}{4} \right) + \frac{3}{2}\pi \right] = 0$$
(16)

and for $\forall p_{12} \in \mathbf{R}^-, \exists k \in \mathbf{Z}$, which satisfies

$$k < -\frac{(p_{12} - a_2)x_2^2}{2\pi a_1 p_{12}} - \frac{3}{4} \tag{17}$$

so that when $x_1 = 2k\pi + \frac{3}{2}\pi$,

$$\dot{V}(x) = (p_{12} - a_2) x_2^2 - a_1 p_{12} x_1 \sin x_1
= (p_{12} - a_2) x_2^2 + a_1 p_{12} x_1
= (p_{12} - a_2) x_2^2 + a_1 p_{12} \left(2k\pi + \frac{3}{2}\pi \right)
> (p_{12} - a_2) x_2^2 + a_1 p_{12} \left[2\pi \left(-\frac{(p_{12} - a_2) x_2^2}{2\pi a_1 p_{12}} - \frac{3}{4} \right) + \frac{3}{2}\pi \right] = 0$$
(18)

In addition, for $p_{12} = 0$, this situation has been discussed in (a). Therefore, the appropriate value for p_{12} to conclude the globally asymptotic stability of the equilibrium point x = 0 with this V(x) can not be found.

Show that if symmetric p.d. matrices P and Q exists such that

$$A^T P + PA + 2\lambda P = -Q \tag{19}$$

then all the eigenvalues of A have a real part strictly less than $-\lambda$.

Solution:

Consider the linear homogeneous continuous-time system

$$\dot{x}(t) = (A + \lambda I) x(t) \tag{20}$$

Let us associate with this system and the equilibrium point $x^* = 0$ the quadratic function

$$V\left(x\right) = x^{T} P x \tag{21}$$

where P is symmetric and positive definite. This V is continuous and has continuous first partial derivatives. Furthermore, since P is positive definite, the origin is the unique minimum point of V. Thus in terms of general characteristics, such a positive definite quadratic form is a suitable candidate for a Lyapunov function. It remains, of course, to determine how $\dot{V}(x)$ is influenced by the dynamics of the system.

We have

$$\dot{V}(x) = \frac{d}{dt}x^{T}Px$$

$$= \dot{x}^{T}Px + x^{T}P\dot{x}$$

$$= x^{T}(A + \lambda I)Px + x^{T}P(A + \lambda I)x$$

$$= x^{T}(A^{T}P + PA + 2\lambda P)x$$

$$= -x^{T}Qx$$
(22)

Because matrix Q is symmetric p.d., $\dot{V}(x) < 0$ for $\forall x \in \mathbf{R} - \{0\}$, indicating that $\dot{V}(x)$ is ND. Therefore, the system is globally asymptotically stable. To ensure the system is global asymptotically stable, the real parts of the eigenvalues of $(A + \lambda I)$ need to be always negative, which means all the eigenvalues of A have a real part strictly less than $-\lambda$ (Luenberger, 1979).

For the linear system

$$\dot{x}_1 = x_2
\dot{x}_2 = -6x_1 - 5x_2$$
(23)

(a) what can you say about its stability and asymptotic stability from the candidate Lyapunov functions

$$V_1(x) = 6x_1^2 + x_2^2$$

$$V_2(x) = x_1^2 + x_2^2 - x_1 x_2$$
(24)

(b) For Q = I, solve the Lyapunov equation for a symmetric p.d. matrix P.

$$A^T P + PA = -Q (25)$$

where

$$A = \begin{bmatrix} 0 & 1 \\ -6 & -5 \end{bmatrix} \tag{26}$$

Solution:

(a) For the candidate V_1 ,

$$V_1(x) = 6x_1^2 + x_2^2 > 0 \text{ for } \forall x \in \mathbf{R}^2 - \left\{ \begin{bmatrix} 0 \\ 0 \end{bmatrix} \right\}$$
 (27)

Therefore, $V_1(x)$ is positive definite. Taking the derivative of Equation (27) yields that

$$\dot{V}_1(x) = 12x_1\dot{x}_1 + 2x_2\dot{x}_2 = 12x_1x_2 + 2x_2(-6x_1 - 5x_2) = -10x_2^2 \le 0$$
 (28)

Therefore, $\dot{V}(x)$ is negative semi-definite, which means the system is stable at the equilibrium point $x = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$.

P.S. If Invariant Set Theorem is used in this question, asymptotic stability can be concluded. Because let $R = \mathbb{R}^2$, if $\dot{V}_1(x) = 0$, $x_2 = 0$, so $\dot{x}_2 = 0$. Substituting $x_2 = 0$ and $\dot{x}_2 = 0$ into Equation (23), we can get $x_1 = 0$. Therefore, $\dot{V}_1(x) = 0$ if and only if $x = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$ Therefore, the system is asymptotically stable.

For the candidate V_2 ,

$$V_2(x) = x_1^2 + x_2^2 - x_1 x_2 = \frac{1}{2} (x_1 - x_2)^2 + \frac{1}{2} x_1^2 + \frac{1}{2} x_2^2 > 0 \text{ for } \forall x \in \mathbf{R}^2 - \left\{ \begin{bmatrix} 0 \\ 0 \end{bmatrix} \right\}$$
 (29)

Therefore, $V_2(x)$ is positive definite. Taking the derivative of Equation (29) yields that

$$\dot{V}_{2}(x) = 2x_{1}\dot{x}_{1} + 2x_{2}\dot{x}_{2} - \dot{x}_{1}x_{2} - x_{1}\dot{x}_{2}$$

$$= 2x_{1}x_{2} + 2x_{2}(-6x_{1} - 5x_{2}) - x_{2}^{2} - x_{1}(-6x_{1} - 5x_{2})$$

$$= 6x_{1}^{2} - 11x_{2}^{2} - 5x_{1}x_{2}$$

$$= (6x_{1} - 11x_{2})(x_{1} + x_{2})$$
(30)

The sign of $\dot{V}_2(x)$ can not be told from Equation (30). Therefore, this candidate Lyapunov functions can not conclude the stability of the equilibrium point x = 0.

(b) Let
$$P = \begin{bmatrix} p_{11} & p_{12} \\ p_{21} & p_{22} \end{bmatrix}$$
, where $p_{12} = p_{21}$.

$$A^{T}P + PA = -Q \Leftrightarrow \begin{bmatrix} 0 & 1 \\ -6 & -5 \end{bmatrix}^{T} \begin{bmatrix} p_{11} & p_{12} \\ p_{21} & p_{22} \end{bmatrix} + \begin{bmatrix} p_{11} & p_{12} \\ p_{21} & p_{22} \end{bmatrix} \begin{bmatrix} 0 & 1 \\ -6 & -5 \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & -1 \end{bmatrix}$$

$$\Leftrightarrow \begin{bmatrix} 0 & -6 \\ 1 & -5 \end{bmatrix} \begin{bmatrix} p_{11} & p_{12} \\ p_{21} & p_{22} \end{bmatrix} + \begin{bmatrix} p_{11} & p_{12} \\ p_{21} & p_{22} \end{bmatrix} \begin{bmatrix} 0 & 1 \\ -6 & -5 \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & -1 \end{bmatrix}$$

$$\Leftrightarrow \begin{bmatrix} -6p_{21} & -6p_{22} \\ p_{11} - 5p_{21} & p_{12} - 5p_{22} \end{bmatrix} + \begin{bmatrix} -6p_{12} & p_{11} - 5p_{12} \\ -6p_{22} & p_{21} - 5p_{22} \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & -1 \end{bmatrix}$$

$$\Leftrightarrow \begin{bmatrix} -6p_{21} - 6p_{12} & -6p_{22} + p_{11} - 5p_{12} \\ p_{11} - 5p_{21} - 6p_{22} & p_{12} - 5p_{22} + p_{21} - 5p_{22} \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & -1 \end{bmatrix}$$

$$\Leftrightarrow \begin{bmatrix} -6p_{21} - 6p_{12} & -6p_{22} + p_{11} - 5p_{12} \\ p_{11} - 5p_{21} - 6p_{22} & p_{12} - 5p_{22} + p_{21} - 5p_{22} \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & -1 \end{bmatrix}$$

$$\Leftrightarrow \begin{bmatrix} (31)$$

Therefore, we can know that

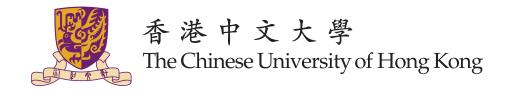
$$\begin{cases}
-6p_{21} - 6p_{12} = -1 \\
-6p_{22} + p_{11} - 5p_{12} = 0 \\
p_{11} - 5p_{21} - 6p_{22} = 0 \\
p_{12} - 5p_{22} + p_{21} - 5p_{22} = -1
\end{cases}$$
(32)

Solving Equation (32) yields that

$$P = \begin{bmatrix} \frac{67}{60} & \frac{1}{12} \\ \frac{1}{12} & \frac{7}{60} \end{bmatrix} \tag{33}$$

References

Luenberger, D. G. (1979). *Introduction to dynamic systems: theory, models, and applications*, volume 1. Wiley New York.



THE CHINESE UNIVERSITY OF HONG KONG

DEPARTMENT OF MECHANICAL & AUTOMATION ENGINEERING

MAEG5070 Nonlinear Control Systems

Assignment #5

by

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2022-23 Term 1

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Determine the stability of the following system at the origin. Indicate whether the stability is asymptotic, and whether it is global.

$$\dot{x}_1 = x_2
\dot{x}_2 = -x_1^3 + \sin^4 x_1 - x_2^7$$
(1)

Solution:

Here we use Lemma 2 of Invariant Set Theorem (Slotine et al., 1991). For the system (1), $c(x_1) = x_1^3 - \sin^4 x_1$ and $b(x_2) = x_2^7$. Therefore,

$$yb(y) = y^8 > 0, y \neq 0$$
 (2)

and

$$yc(y) = y\left(y^3 - \sin^4 y\right) \tag{3}$$

Let $f(x) = x^3 - \sin^4 x$.

$$f'(x) = -4\sin^3 x \cos x + 3x^2 \tag{4}$$

Because $\sin x \cos x \le \frac{\sin^2 x + \cos^2 x}{2} = \frac{1}{2}$ (Cauchy–Schwarz inequality),

$$f'(x) = -4\sin^2 x \sin x \cos x + 3x^2 \ge -\sin^2 x + 3x^2 \ge -2x^2 = 3x^2 = x^2 \ge 0$$
 (5)

Hence, f(x) is a monotonically increase function, And we note that f(0) = 0. Therefore, f(x) > 0 when x > 0 and f(x) < 0 when x < 0. Therefore, we can conclude that

$$yc(y) = y\left(y^3 - \sin^4 y\right) > 0 \tag{6}$$

Hence, the system is asymptotically stable at the equilibrium point x = 0.

Moreover,

$$\lim_{|y| \to \infty} \int_0^y c(r) dr = \lim_{|y| \to \infty} \int_0^y \left(r^3 - \sin^4 r \right) dr > \lim_{|y| \to \infty} \int_0^y r^3 dr = \lim_{|y| \to \infty} \frac{1}{4} y^4 = \infty$$
 (7)

Hence, the system is globally asymptotically stable at the equilibrium point x = 0.

Consider Lienard's equation

$$\dot{x}_1 = x_2
\dot{x}_2 = -x_2 \sin^2 x_1 - b(x_1)$$
(8)

where b(y) is continuous function over $y \in \mathbf{R}$ and satisfies yb(y) > 0, $y \neq 0$.

(a) Show the following function

$$V(x_1, x_2) = \frac{1}{2}x_2^2 + \int_0^{x_1} b(y) dy$$
 (9)

is a Lyapunov function for the system.

- (b) Show that the origin is locally asymptotically stable.
- (c) Can you conclude global asymptotic stability of the origin based on this Lyapunov function? Why?

Solution:

(a) Because yb(y) > 0, b(y) > 0 for y > 0 and b(y) < 0 for y < 0. Hence, $\int_0^{x_1} b(y) dy > 0$ for $x_1 \neq 0$. Therefore,

$$V(x_1, x_2) = \frac{1}{2}x_2^2 + \int_0^{x_1} b(y) \, dy > 0 \tag{10}$$

Taking the derivative of Equation (9) gets

$$\dot{V}(x_1, x_2) = \frac{\partial V(x)}{\partial x_1} \dot{x}_1 + \frac{\partial V(x)}{\partial x_2} \dot{x}_2
= b(x_1) x_2 + x_2 \left(-x_2 \sin^2 x_1 - b(x_1) \right)
= x_2^2 \sin^2 x_1 \le 0$$
(11)

Therefore, V(x) is positive definite, and $\dot{V}(x)$ is negative-semi definite, from which we can conclude that

$$V(x_1, x_2) = \frac{1}{2}x_2^2 + \int_0^{x_1} b(y) dy$$
 (12)

is a Lyapunov function for the system.

- (b) Invariant Set Theorem is used in this question. For $x_1 \in (-\pi, \pi) \{0\}$, if $\dot{V}(x_1, x_2) = 0$, $x_2 = 0$, so $\dot{x}_2 = 0$. Substituting $x_2 = 0$ and $\dot{x}_2 = 0$ into Equation (8), we can get $x_1 = 0$. Therefore, $\dot{V}_1(x) = 0$ if and only if $x = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$ for $\{(x_1, x_2) \mid -\pi < x_1 < \pi, x_2 \in \mathbf{R}\}$. Therefore, the system is locally asymptotically stable.
- (c) Global asymptotic stability of the origin based on this Lyapunov function can **not** be concluded because $\dot{V}(x_1, x_2) = 0$ when $\{(x_1, x_2) | x_1 = k\pi, k \in \mathbf{Z}, x_2 \in \mathbf{R}\}$ so we cannot find the invariant set.

Using the Krasovskii Theorem to show the global asymptotic stability of the equilibrium point at the origin of the following system

$$\dot{x}_1 = -3x_1 + x_2
\dot{x}_2 = x_1 - 3x_2 - x_2^5$$
(13)

Solution:

$$\frac{\partial f}{\partial x} = \begin{bmatrix} -3 & 1\\ 1 & -3 - 5x_2^4 \end{bmatrix} \tag{14}$$

$$F(x) = \frac{\partial f}{\partial x} + \frac{\partial f^{T}}{\partial x} = \begin{bmatrix} -6 & 2\\ 2 & -6 - 10x_{2}^{4} \end{bmatrix} < 0, \forall x$$
 (15)

Thus, the equilibrium point is asymptotic stable.

Moreover,

$$V(x) = f^{T}(x) f(x) = (-3x_1 + x_2)^2 + \left(x_1 - 3x_2 - x_2^5\right)^2$$
(16)

is radially unbounded. Thus, the equilibrium point is global asymptotic stable.

Consider the following system:

$$\dot{x}_1 = x_2
\dot{x}_2 = -c(x_1) - b(x_2)$$
(17)

where the functions c and b are continuous satisfying the sign condition. Using the variable gradient method to derive a Lyapunov function for Equation (17) as follows:

$$V(x_1, x_2) = \int_0^{x_1} c(y) dy + \frac{1}{2} x_2^3$$
 (18)

Solution:

Let $\nabla V = [a_1c(x_1), a_2x_2]$. Because

$$\frac{\partial \nabla V_1}{x_2} = \frac{\partial a_1 c(x_1)}{x_2} = 0 = \frac{\partial a_2 x_2}{x_1} = \frac{\partial \nabla V_2}{x_1}$$
 (19)

we can make $a_1 = a_2 = 1$. Then, \dot{V} can be computed as

$$\dot{V} = \nabla V \dot{x} = c(x_1) x_2 + x_2 (-c(x_1) - b(x_2)) = -x_2 b(x_2)$$
(20)

Because b is continuous satisfying the sign condition, $\dot{V} < 0$, which means \dot{V} is negative definite. Therefore, the Lyapunov function can be expressed as

$$V(x) = \int_0^{x_1} \nabla V_1(x_1, 0) dx_1 + \int_0^{x_2} \nabla V_2(x_1, x_2) dx_2$$

$$= \int_0^{x_1} c(x_1) dx_1 + \int_0^{x_2} x_2 dx_2$$

$$= \int_0^{x_1} c(y) dy + \frac{1}{2}x_2^2$$
(21)

References

Slotine, J.-J. E., Li, W., et al. (1991). *Applied nonlinear control*, volume 199. Prentice hall Englewood Cliffs, NJ.



THE CHINESE UNIVERSITY OF HONG KONG

DEPARTMENT OF MECHANICAL & AUTOMATION ENGINEERING

MAEG5070 Nonlinear Control Systems

Assignment #6

by

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Liuchao Gin

2022-23 Term 1

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Show that the one-dimensional system $\dot{x} = -a(t)x$ where a(t) is continuous and nonnegative over $t \ge 0$ is exponentially stable if there exist a T > 0 such that, for any t > 0, $\int_t^{t+T} a(r) dr \ge \gamma$ for some $\gamma > 0$.

Hint: For any $t \ge t_0$, $e^{-\int_t^{t+T} a(r)dr} \le e^{-\gamma} < 1$.

Solution:

For the system, $\dot{x} = -a(t)x$, the solution for x(t) is

$$x(t) = x(t_0) e^{-\int_{t_0}^t a(x)dx}$$
 (1)

If for any t > 0, $\int_{t}^{t+T} a(r) dr \ge \gamma$ for some $\gamma > 0$,

$$\int_{t_0}^{t} a(\tau) d\tau = \int_{t_0}^{t+T} a(\tau) d\tau + \int_{t_0+T}^{t_0+2T} a(\tau) d\tau + \dots + \int_{t-T}^{t} a(\tau) d\tau \ge \frac{t-t_0}{T} \gamma \qquad (2)$$

Therefore,

$$e^{-\int_{t_0}^t a(x)dx} \le e^{-\frac{t-t_0}{T}\gamma} \tag{3}$$

Hence,

$$x(t) = x(t_0) e^{-\int_{t_0}^t a(x)dx} \le x(t_0) e^{\frac{t_0}{T}\gamma} e^{-\frac{\gamma}{T}t}$$
(4)

We can conclude that $\dot{x} = -a(t)x$ is exponentially stable.

Condition (4.19) on the eigenvalues of $A(t) + A^{T}(t)$ is only, of course, a sufficient condition. For instance, show that the linear time-varying system associated with the matrix

$$\mathbf{A}\left(t\right) = \begin{bmatrix} -1 & e^{t/2} \\ 0 & -1 \end{bmatrix} \tag{5}$$

is globally asymptotically stable.

Solution:

$$\mathbf{A}(t) = \begin{bmatrix} -1 & e^{t/2} \\ 0 & -1 \end{bmatrix} \Longrightarrow \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -x_1 + e^{\frac{t}{2}} x_2 \\ -x_2 \end{bmatrix}$$
 (6)

we can obtain the solution for $x_2(t)$:

$$x_2(t) = x_2(t_0) e^{-(t-t_0)}$$
(7)

Because $\dot{x}_1 = -x_1 + e^{\frac{t}{2}}x_2$

$$x_{1}(t) = x_{1}(t_{0}) e^{-(t-t_{0})} + \int_{t_{0}}^{t} e^{-(t-\tau)} e^{\frac{\tau}{2}} x_{2}(\tau) d\tau$$

$$= x_{1}(t_{0}) e^{-(t-t_{0})} + \int_{t_{0}}^{t} e^{-(t-\tau)} e^{\frac{\tau}{2}} x_{2}(t_{0}) e^{-(\tau-t_{0})} d\tau$$

$$= x_{1}(t_{0}) e^{-(t-t_{0})} + x_{2}(t_{0}) e^{-(t-t_{0})} \int_{t_{0}}^{t} e^{\frac{\tau}{2}} d\tau$$

$$= x_{1}(t_{0}) e^{-(t-t_{0})} + 2x_{2}(t_{0}) e^{-(t-t_{0})} \left(e^{\frac{t}{2}} - e^{\frac{t_{0}}{2}} \right)$$

$$= x_{1}(t_{0}) e^{-(t-t_{0})} + 2x_{2}(t_{0}) e^{-(\frac{t}{2}-t_{0})} - 2x_{2}(t_{0}) e^{-(t-\frac{3}{2}t_{0})}$$

$$(8)$$

We can conclude that $\dot{x} = -A(t)x$ is globally asymptotically stable since $\lim_{t\to\infty} x_i(t) = 0$, i = 1, 2.

Determine whether the following systems have a stable equilibrium. Indicate whether the stability is asymptotic, and whether it is global.

(a)
$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -10 & e^{3t} \\ 0 & -2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$
 (9)

(b)
$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -1 & 2\sin t \\ 0 & -(t+1) \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$
 (10)

(c)
$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -1 & e^{2t} \\ 0 & -2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$
 (11)

Solution:

(a)
$$A(t) = \begin{bmatrix} -10 & e^{3t} \\ 0 & -2 \end{bmatrix} \Longrightarrow \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -10x_1 + e^{3t}x_2 \\ -2x_2 \end{bmatrix}$$
 (12)

we can obtain the solution for $x_2(t)$:

$$x_2(t) = x_2(t_0) e^{-2(t-t_0)}$$
 (13)

Because $\dot{x}_1 = -10x_1 + e^{3t}x_2$

$$x_{1}(t) = x_{1}(t_{0}) e^{-10(t-t_{0})} + \int_{t_{0}}^{t} e^{-10(t-\tau)} e^{3\tau} x_{2}(\tau) d\tau$$

$$= x_{1}(t_{0}) e^{-(t-t_{0})} + \int_{t_{0}}^{t} e^{-10(t-\tau)} e^{3\tau} x_{2}(t_{0}) e^{-2(\tau-t_{0})} d\tau$$

$$= x_{1}(t_{0}) e^{-(t-t_{0})} + x_{2}(t_{0}) e^{-(10t-2t_{0})} \int_{t_{0}}^{t} e^{11\tau} d\tau$$

$$= x_{1}(t_{0}) e^{-(t-t_{0})} + \frac{1}{11} x_{2}(t_{0}) e^{-(t-2t_{0})} \left(e^{11t} - e^{11t_{0}} \right)$$

$$= x_{1}(t_{0}) e^{-(t-t_{0})} + \frac{1}{11} x_{2}(t_{0}) e^{t+3t_{0}} - \frac{1}{11} x_{2}(t_{0}) e^{-(10t-13t_{0})}$$

$$(14)$$

We can conclude that $\dot{x} = -A(t)x$ is unstable since $\lim_{t\to\infty} x_1(t) = \infty$.

(b)
$$A(t) + A^{T}(t) = \begin{bmatrix} -2 & 2\sin t \\ 2\sin t & -2(t+1) \end{bmatrix} \Longrightarrow -\left(A(t) + A^{T}(t)\right) = \begin{bmatrix} 2 & -2\sin t \\ -2\sin t & 2(t+1) \end{bmatrix}$$
(15)

The determinant of $-(A(t) + A^{T}(t))$ is equal to

$$\det \left[-\left(A\left(t\right) +A^{T}\left(t\right) \right) \right] =4\left(t+1\right) -4\sin ^{2}t\geq 4\left(t+1\right) -4t>0 \tag{16}$$

Therefore, $-(A(t) + A^T(t))$ is positive definite, which means $A(t) + A^T(t)$ is negative definite. Hence, $\lambda_i(A(t) + A^T(t)) < -\lambda$ for some $\lambda > 0$. We can conclude that the system is globally asymptotically stable.

(c) $\mathbf{A}(t) = \begin{bmatrix} -1 & e^{2t} \\ 0 & -2 \end{bmatrix} \Longrightarrow \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -1x_1 + e^{2t}x_2 \\ -2x_2 \end{bmatrix}$ (17)

we can obtain the solution for $x_2(t)$:

$$x_2(t) = x_2(t_0) e^{-2(t-t_0)}$$
 (18)

Because $\dot{x}_1 = -10x_1 + e^{3t}x_2$

$$x_{1}(t) = x_{1}(t_{0}) e^{-(t-t_{0})} + \int_{t_{0}}^{t} e^{-(t-\tau)} e^{3\tau} x_{2}(\tau) d\tau$$

$$= x_{1}(t_{0}) e^{-(t-t_{0})} + \int_{t_{0}}^{t} e^{-(t-\tau)} e^{2\tau} x_{2}(t_{0}) e^{-2(\tau-t_{0})} d\tau$$

$$= x_{1}(t_{0}) e^{-(t-t_{0})} + x_{2}(t_{0}) e^{-(t-2t_{0})} \int_{t_{0}}^{t} e^{\tau} d\tau$$

$$= x_{1}(t_{0}) e^{-(t-t_{0})} + x_{2}(t_{0}) e^{-(t-2t_{0})} (e^{t} - e^{t_{0}})$$

$$= x_{1}(t_{0}) e^{-(t-t_{0})} + x_{2}(t_{0}) e^{t_{0}} - x_{2}(t_{0}) e^{-(t-3t_{0})}$$

$$= x_{1}(t_{0}) e^{-(t-t_{0})} + x_{2}(t_{0}) e^{t_{0}} - x_{2}(t_{0}) e^{-(t-3t_{0})}$$

$$= x_{1}(t_{0}) e^{-(t-t_{0})} + x_{2}(t_{0}) e^{t_{0}} - x_{2}(t_{0}) e^{-(t-3t_{0})}$$

Since we can find constant $r(R, t_0) = \frac{R}{4}e^{-3t_0}$, $\forall R > 0$, such that $||x(t_0)|| < r \Rightarrow ||x(t)|| < R$, $t \ge t_0$, so, the equilibrium point at origin is stable.

However, $\lim_{t\to\infty} x_1(t) = x_2(t_0) e^{t_0}$, so it is not asymptotically stable.

Show that the following system is globally exponentially stable with a detailed argument.

$$\dot{x}_1 = -\left(5 + x_2^5 + x_3^8\right) x_1
\dot{x}_2 = -x_2 + 4x_3^2
\dot{x}_3 = -\left(2 + \sin t\right) x_3$$
(20)

Solution:

Let $a(t) = 2 + \sin t$. Then

$$x_3(t) = x_3(t_0) e^{-\int_{t_0}^t (2+\sin\tau)d\tau} \Longrightarrow ||x_3|| e^{-(t-t_0)}$$
 (21)

Therefore,

$$x_2(t) = e^{-(t-t_0)} x_2(t_0) + \int_{t_0}^t e^{-(t-\tau)} 4x_3^2(\tau) d\tau$$
 (22)

Thus, it is ready to see that the system is globally exponentially stable upon using Proposition 1 on the x_1 subsystem (Slotine et al., 1991).

- (i) For the autonomous system $\dot{x} = f(x), x \in \mathbb{R}^n$, show that, if, in a certain neighborhood Ω of the origin, there exists a continuously differentiable scalar function V(x) such that
 - $V(0) = 0 \quad \forall t \ge 0$
 - V(x) can assume strictly positive values arbitrarily close to the origin.
 - $\dot{V}(x)$ is positive definite (locally in Ω)

then the equilibrium point 0 is unstable.

(ii) Show that the E.P. of $\dot{x} = c(x)$ is unstable where c(x) is continuous and satisfies $xc(x) > 0, x \neq 0$.

Hint: Let R > 0 be such that \dot{V} is P.D. on $B_R = \{x | ||x||^2 \le R^2\}$ and $B_R \subset \Omega$, and let

$$M = \max_{x \in B_R} V(x) \tag{23}$$

V is continuous & B_R compact $\Longrightarrow M$ exists. Also, M>0 since V(x) can assume strictly positive values arbitrarily close to the origin. For any R>r>0, there exists x(0) such that $0<\|x(0)\|< r$, and V(x(0))=a>0. Since $\dot{V}(x)$ is positive definite (locally in Ω), V(x(t))>V(x(0))>0 for all $t\geq 0$. Let $U=\{x|x\in B_R \text{ and } V(x)\}\geq a$. Then U is compact. Thus there exists L>0 such that

$$L = \min_{x \in U} \left\{ \dot{V} \right\} \tag{24}$$

If $||x(t, x_0)|| < R$ for all $t \ge 0$, then

$$V(x(t,x_{0})) - V_{0}(x_{0}) = \int_{0}^{t} \dot{V}(x(t,x_{0})) dt \ge \int_{0}^{t} L dt = Lt$$

$$\Longrightarrow V(x(t,x_{0})) \ge V_{0}(x_{0}) + Lt > M$$
(25)

when $t > \frac{M-V(x_0)}{L}$ which contradicts Equation (23). Thus, the E.P. is unstable.

Solution:

(i) Let R > 0 be such that \dot{V} is P.D. on $B_R = \{x | ||x||^2 \le R^2\}$ and $B_R \subset \Omega$, and let

$$M = \max_{x \in B_R} V(x) \tag{26}$$

V is continuous & B_R compact $\Longrightarrow M$ exists. Also, M>0 since V(x) can assume strictly positive values arbitrarily close to the origin. For any R>r>0, there exists x(0) such that $0<\|x(0)\|< r$, and V(x(0))=a>0. Since $\dot{V}(x)$ is positive definite (locally in Ω), V(x(t))>V(x(0))>0 for all $t\geq 0$. Let $U=\{x|x\in B_R \text{ and } V(x)\}\geq a$. Then U is compact. Thus there exists L>0 such that

$$L = \min_{x \in U} \left\{ \dot{V} \right\} \tag{27}$$

If $||x(t, x_0)|| < R$ for all $t \ge 0$, then

$$V(x(t,x_0)) - V_0(x_0) = \int_0^t \dot{V}(x(t,x_0)) dt \ge \int_0^t Ldt = Lt$$

$$\implies V(x(t,x_0)) \ge V_0(x_0) + Lt > M$$
(28)

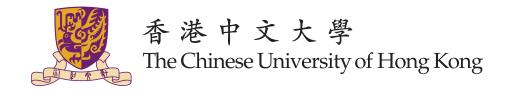
when $t > \frac{M - V(x_0)}{L}$ which contradicts Equation (23). Thus, the E.P. is unstable.

(ii) If we take $V(x) = x^2$, we can see that V(0) = 0 $\forall t \ge 0$. And $\dot{V}(x) = 2x\dot{x} = 2xc(x) > 0$, $\forall x \ne 0$, so \dot{V} is globally positive definite.

Therefore, the equilibrium point of $\dot{x} = c(x)$ is unstable.

References

Slotine, J.-J. E., Li, W., et al. (1991). *Applied nonlinear control*, volume 199. Prentice hall Englewood Cliffs, NJ.



THE CHINESE UNIVERSITY OF HONG KONG

DEPARTMENT OF MECHANICAL & AUTOMATION ENGINEERING

MAEG5070 Nonlinear Control Systems

Assignment #7

by

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Liuchao Gin

2022-23 Term 1

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Show that if a function $x:[0,\infty)\to R^n$ is uniformly continuous, and there exists a positive definite quadratic function V(x) such that

$$\int_{0}^{\infty} V(x(t)) dt < 0 \tag{1}$$

then x(t) tends to zero as $t \to \infty$.

Solution:

Because V(x) is a positive definite quadratic function, we can express V(x(t)) as follows

$$V\left(x\left(t\right)\right) = x^{T} P x \tag{2}$$

where *P* is a positive definite matrix.

Define $f(t) = \int_0^t x(\tau) d\tau$. We claim that f(t) has a finite limit as $t \to \infty$. Otherwise, if

$$\lim_{t \to \infty} f(t) = \int_0^\infty x(\tau) d\tau = \infty$$
 (3)

we will have

$$\int_0^\infty \|x(\tau)\|^2 d\tau = \infty \tag{4}$$

In addition,

$$\int_0^\infty \|x(\tau)\|^2 d\tau \le \lambda_{max}(P) \int_0^\infty x^T P x dt = \lambda_{max}(P) \int_0^\infty V(x(t)) dt \tag{5}$$

Hence,

$$\int_{0}^{\infty} V(x(t)) dt = \infty$$
 (6)

which is contradicted to Equation (1). Therefore, f(t) has a finite limit as $t \to \infty$.

Besides, because $x:[0,\infty)\to R^n$ is uniformly continuous, that is $\dot{f}(t)$ is uniformly continuous, by Barbalat's Lemma 4.2, we can conclude that $\dot{f}(t)\to 0$ as $t\to 0$, that is x(t) tends to zero as $t\to \infty$.

Consider the following one dimensional single-input nonlinear control system

$$\dot{x} = \theta g\left(x, t\right) + u \tag{7}$$

where θ is some constant parameter, and g(x,t) is some bounded smooth function defined for all t and x.

(a) Assuming θ is known, show that, under the following state feedback nonlinear controller

$$u = -\theta g(x, t) - kx \tag{8}$$

where k > 0, the equilibrium point of the closed-loop system is globally asymptotically stable.

(b) If θ is unknown, the feedback controller $u = -\theta g(x, t) - kx$ is not implementable. One can use adaptive control to control the system. Show that, under the following adaptive controller

$$u = -\hat{\theta}g(x,t) - kx$$

$$\dot{\hat{\theta}} = g(x,t)x$$
(9)

the closed-loop system takes the following form

$$\dot{x} = \phi g(x, t) - kx
\dot{\hat{\theta}} = g(x, t) x$$
(10)

where $\phi = \theta - \hat{\theta}$ (you can interpret $\hat{\theta}$ as an estimation of θ).

- (c) Using a Lyapunov-like function $V = x^2 + \phi^2$ to show that both x and $\hat{\theta}$ are bounded and $\lim_{t\to\infty} x(t) = 0$.
- (d) For g(x,t) = cos(x) sin(t) and k = 2, do the simulation for the closed-loop system using MATLAB with x(0) = 0 and $\hat{\theta}(0) = 1$. Plot x(t); $\hat{\theta}(t)$; $\phi(t)$; u(t) for 0 < t < 40 seconds.

Solution:

(a) Substituting the controller in Equation (8) into the system in Equation (7) yields that

$$\dot{x} = \theta g(x, t) + u = \theta g(x, t) - \theta g(x, t) - kx = -kx \tag{11}$$

Because k > 0, according to linear system stability theory, -k is Hurwitz. Therefore, the equilibrium point of the closed-loop system is globally asymptotically stable.

(b) Substituting the controller in Equation (9) into the system in Equation (7) yields that

$$\dot{x} = \theta g(x, t) + u$$

$$u = -\hat{\theta} g(x, t) - kx \implies \dot{\hat{\theta}} = g(x, t) x$$

$$\dot{\hat{\theta}} = g(x, t) x$$

$$\dot{\hat{\theta}} = g(x, t) x$$
(12)

where $\phi = \theta - \hat{\theta}$ (you can interpret $\hat{\theta}$ as an estimation of θ).

(c) $V = x^2 + \phi^2$ is lower bounded obviously. And its derivative

$$\dot{V} = 2x\dot{x} + 2\phi\dot{\phi}
= 2x (\phi g(x,t) - kx) + 2\phi (\dot{\theta} - \dot{\theta})
= 2x (\phi g(x,t) - kx) + 2\phi (0 - g(x,t)x)
= -2kx^{2} < 0$$
(13)

This implies that $V(x(t)) \le V(x(0))$, $\forall t > 0$, which indicate that x and ϕ should all be bounded. Taking the derivative to \dot{V} yields that

$$\ddot{V} = -4kx\dot{x} = -4kx\left(\phi g\left(x,t\right) - kx\right) \tag{14}$$

Here, x, ϕ , and g(x, t) are all bounded. Therefore, \ddot{V} is bounded. According to Barbalat's Lemma 4.1, \dot{V} is uniformly continuous. Again, using Barbalat's Lemma 4.3, $\dot{V}(x, t) \to 0$ as $t \to \infty$, which means $\lim_{t \to \infty} x(t) = 0$.

(d) We set $\theta = \pi$ and use following Simulink to get the results:

And we use the following code to plot the results:

```
1 clear all; clc;
2 figg1 = openfig('x.fig','reuse');
3 grid on;
4 xlabel('$t, \mathrm{\ \left(s\right)}$','interpreter','latex');
5 ylabel('$x, \mathrm{\ \left(m\right)}$', 'interpreter','latex');
6 title('');
7 a = get(gca,'XTickLabel');
8 set(gca,'XTickLabel',a,'FontName','Times','fontsize',12);
9 set(gcf,'renderer','painters');
10 filename = "x"+".pdf";
11 saveas(gcf, filename);
12 close(figg1);
13 figg2 = openfig('theta.fig','reuse');
15 xlabel('$t, \mathrm{\ \left(s\right)}$','interpreter','latex');
16 ylabel('$\hat{\theta}$', 'interpreter','latex');
17 title('');
18 a = get(gca,'XTickLabel');
```

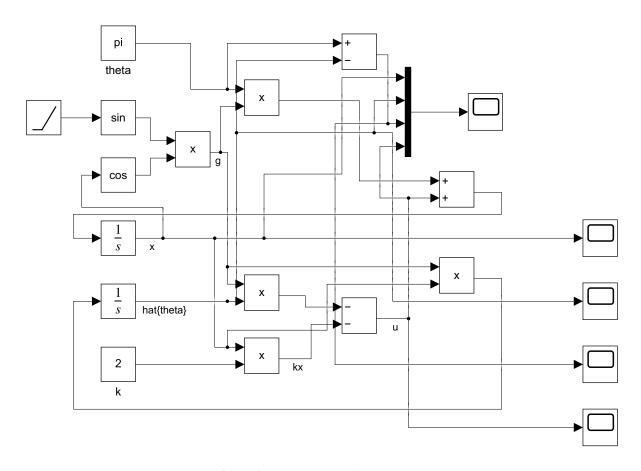


Figure 1: Block diagram for the system.

```
19 set(gca,'XTickLabel',a,'FontName','Times','fontsize',12);
20 set(gcf,'renderer','painters');
21 filename = "theta"+".pdf";
22 saveas (gcf, filename);
23 close(figg2);
24 figg3 = openfig('phi.fig','reuse');
25 grid on;
26 xlabel('$t, \mathrm{\\left(s\right)}$','interpreter','latex');
27 ylabel('$\phi$', 'interpreter','latex');
28 title('');
29 a = get(gca,'XTickLabel');
30 set(gca,'XTickLabel',a,'FontName','Times','fontsize',12);
31 set(gcf,'renderer','painters');
32 filename = "phi"+".pdf";
33 saveas(gcf, filename);
34 close(figg3);
35 figg4 = openfig('u.fig','reuse');
36 grid on;
37 xlabel('$t, \mathrm{\ \left(s\right)}$','interpreter','latex');
38 ylabel('$u$', 'interpreter','latex');
39 title('');
40 a = get(gca,'XTickLabel');
```

```
41 set(gca,'XTickLabel',a,'FontName','Times','fontsize',12);
42 set(gcf,'renderer','painters');
43 filename = "u"+".pdf";
44 saveas(gcf,filename);
45 close(figg4);
```

The results are shown as follows:

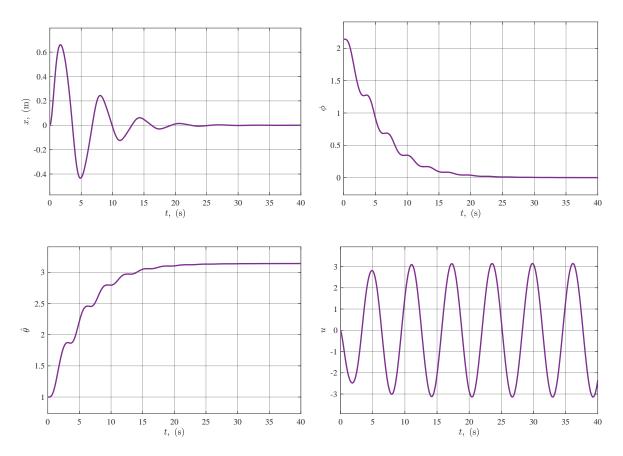


Figure 2: Simulation results.

Consider the system $\dot{x} = f(x)$ where $x \in \mathbb{R}^n$, and f is continuously differentiable with f(0) = 0. Let J be the Jacobian matrix of f at the origin. It is known from the Lyapunov's linearization method that the equilibrium at x = 0 of this system is unstable if at least one of the eigenvalues of J has positive real part. Prove a special case of this result by assuming that n = 2 and

$$J = \begin{bmatrix} 1 & 0 \\ 0 & -2 \end{bmatrix}$$

Hint: Let $V(x) = x_1^2 - x_2^2$.

Solution:

Because $J = \begin{bmatrix} 1 & 0 \\ 0 & -2 \end{bmatrix}$, the system can be described as

$$\begin{cases} \dot{x}_1 = x_1 + g_1(x_1, x_2) \\ \dot{x}_2 = -2x_2 + g_2(x_1, x_2) \end{cases}$$
 (15)

where $g_1(x_1, x_2)$ and $g_2(x_1, x_2)$ are higher order terms.

Define $V(x) = x_1^2 - x_2^2$ satisfies V(0) = 0 and we can assume positive values arbitrarily near the origin. Take the time derivative to V(x):

$$\dot{V}(x) = 2x_1\dot{x}_1 - 2x_2\dot{x}_2
= 2x_1(x_1 + g_1(x_1, x_2)) - 2x_2(-2x_2 + g_2(x_1, x_2))
= 2x_1^2 + 4x_2^2 + 2x_1g_1(x_1, x_2) - 2x_2g_2(x_1, x_2)$$
(16)

Because $g_1(x_1, x_2)$ and $g_2(x_1, x_2)$ are higher order terms, $\forall \alpha_{1,2} > 0$, $\exists r > 0$ such that $\|g_i(x_1, x_2)\| < \alpha_i \|x_i\|$, i = 1, 2, $\forall x \in B_r$. Therefore,

$$\dot{V}(x) = 2x_1^2 + 4x_2^2 + 2x_1g_1(x_1, x_2) - 2x_2g_2(x_1, x_2)
\ge 2||x_1||^2 + 4||x_2||^2 - 2\alpha_1||x_1||^2 - 2\alpha_2||x_2||^2
= (2 - 2\alpha_1) ||x_1||^2 + (4 - 2\alpha_2) ||x_2||^2$$
(17)

as long as we select $0 < \alpha_1 < 1$ and $0 < \alpha_2 < \frac{1}{2}$, $\dot{V}(x)$ can defined as positive definite in B_r .

Consider the second order system

$$\dot{x}_1 = x_1 x_2
\dot{x}_2 = x_1 + u$$
(18)

using backstepping to design a state feedback controller to globally stabilize the origin.

Solution:

Letting $u = u_a - x_1$ gives

$$\dot{x}_1 = x_1 x_2
\dot{x}_2 = u_a$$
(19)

In this form, $\eta = x_1$ and $\zeta = x_2$.

$$f(\eta) = 0 \tag{20}$$

and

$$g(\eta) = \eta \tag{21}$$

Therefore,

$$\phi(x_1) = \frac{-\alpha \eta - f(\eta)}{g(\eta)} = -\alpha \tag{22}$$

Here, $\alpha > 0$. The closed-loop system has a control Lyapunov function

$$V(x_1) = \frac{1}{2}x_1^2 \tag{23}$$

By Lemma 1, we can have a control Lyapunov function

$$V_{\alpha}(x_1, x_2) = V(x_1) + \frac{1}{2}(x_2 - \phi(x_1))^2$$

$$= \frac{1}{2}x_1^2 + \frac{1}{2}(x_2 + \alpha)^2$$
(24)

with respect to

$$u_{a} = \phi_{\alpha}(x_{1}, x_{2})$$

$$= \frac{\partial \phi(\eta)}{\partial \eta} [f(\eta) + g(\eta) \zeta] - \frac{\partial V(\eta)}{\partial \eta} g(\eta) - k(\zeta - \phi(\eta)) = -x_{1}^{2} - k(x_{2} + \alpha)$$
(25)

where k > 0. Therefore,

$$u = u_a - x_1 = -x_1^2 - x_1 - k(x_2 + \alpha)$$
(26)

(a) Using the Lyapunov function candidate $V(x) = x^2$ to determine the stability of the origin of the following system

$$\dot{x} = -x^3 + x^2 \sin^2 x \tag{27}$$

(b) Using backstepping to design a state feedback controller to globally stabilize the origin of the following system

$$\dot{x}_1 = -x_1^3 + x_1 x_2 \sin^2 x_1
\dot{x}_2 = x_3
\dot{x}_3 = x_3 + \exp(x_2)u$$
(28)

Solution:

(a) $V(x) = x^2$ is positive definite. Taking the time derivative to V(x) yields

$$\dot{V}(x) = 2x\dot{x} = 2x\left(-x^3 + x^2\sin^2 x\right) = -2\left(x^4 - x^3\sin^2 x\right) < -2\left(x^4 - x^3x\right) = 0$$
 (29)

Hence, $\dot{V}(x)$ is negative definite. Therefore, the system is globally asymptotically stable.

(b) Letting $u = \exp(-x_2) (u_a - x_3)$ gives

$$\dot{x}_1 = -x_1^3 + x_1 x_2 \sin^2 x_1
\dot{x}_2 = x_3
\dot{x}_3 = u_a$$
(30)

In this form, $\eta = x_1$ and $\zeta = x_2$.

$$f(\eta) = -x_1^3 \tag{31}$$

and

$$g(\eta) = x_1 \sin^2 x_1 \tag{32}$$

From part (a), we can have a control Lyapunov function

$$V(x_1) = \frac{1}{2}x_1^2 \tag{33}$$

with respect to

$$\phi\left(x_{1}\right) = x_{1} \tag{34}$$

By Lemma 1, we can have a control Lyapunov function

$$V_{\alpha}(x_1, x_2) = V(x_1) + \frac{1}{2}(x_2 - \phi(x_1))^2$$

$$= \frac{1}{2}x_1^2 + \frac{1}{2}(x_2 - x_1)^2$$
(35)

with respect to

$$\phi_{\alpha}(x_{1}, x_{2})$$

$$= \frac{\partial \phi(\eta)}{\partial \eta} \left[f(\eta) + g(\eta) \zeta \right] - \frac{\partial V(\eta)}{\partial \eta} g(\eta) - k(\zeta - \phi(\eta))$$

$$= -x_{1}^{3} + x_{1}x_{2} \sin^{2} x_{1} - x_{1}^{2} \sin^{2} x_{1} - k_{1}(x_{2} - x_{1})$$
(36)

where $k_1 > 0$. Applying the extension of Lemma 1 to the whole system yields

$$V(x_1, x_2, x_3) = V_{\alpha}(x_1, x_2) + \frac{1}{2}(x_3 - \phi(x_1, x_2))^2$$

$$= \frac{1}{2}x_1^2 + \frac{1}{2}(x_2 - x_1)^2$$

$$+ \frac{1}{2}(x_3 + x_1^3 - x_1x_2\sin^2 x_1 + x_1^2\sin^2 x_1 + k_1(x_2 - x_1))^2$$
(37)

with respect to

$$u_{a} = \phi_{\alpha} (x_{1}, x_{2}, x_{3})$$

$$= \frac{\partial \phi_{\alpha} (x_{1}, x_{2})}{\partial (x_{1}, x_{2})} [f (x_{1}, x_{2}) + g (x_{1}, x_{2}) x_{3}] - \frac{\partial V_{\alpha} (x_{1}, x_{2})}{\partial (x_{1}, x_{2})} g (x_{1}, x_{2}) - k (x_{3} - \phi_{\alpha} (x_{1}, x_{2}))$$

$$= \left(-3x_{1}^{2} + x_{2} \sin^{2} x_{1} + 2x_{1}x_{2} \sin x_{1} \cos x_{1} - 2x_{1} \sin^{2} x_{1} - 2x_{1}^{2} \sin x_{1} \cos x_{1} + k_{1}\right) \left(-x_{1}^{3} + x_{1}x_{2} \sin^{2} x_{1}\right)$$

$$+ \left(x_{1} \sin^{2} x_{1} + k_{1}\right) x_{3} - (x_{2} - x_{1}) - k_{2} \left(x_{3} + x_{1}^{3} - x_{1}x_{2} \sin^{2} x_{1} + x_{1}^{2} \sin^{2} x_{1} + k_{1} (x_{2} - x_{1})\right)$$
(38)

Therefore,

$$u = \exp(-x_2) (u_a - x_3)$$

$$= \exp(-x_2) \left(-3x_1^2 + x_2 \sin^2 x_1 + 2x_1 x_2 \sin x_1 \cos x_1 - 2x_1 \sin^2 x_1 - 2x_1^2 \sin x_1 \cos x_1 + k_1 \right)$$

$$\cdot \left(-x_1^3 + x_1 x_2 \sin^2 x_1 \right) + \exp(-x_2) \left(x_1 \sin^2 x_1 + k_1 \right) x_3 - \exp(-x_2) (x_2 - x_1)$$

$$- k_2 \exp(-x_2) \left(x_3 + x_1^3 - x_1 x_2 \sin^2 x_1 + x_1^2 \sin^2 x_1 + k_1 (x_2 - x_1) \right)$$
(39)



THE CHINESE UNIVERSITY OF HONG KONG

DEPARTMENT OF MECHANICAL & AUTOMATION ENGINEERING

MAEG5070 Nonlinear Control Systems

Assignment #8

by

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Liuchao Gin

2022-23 Term 1

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Consider the controlled van del Pol equation

$$\dot{x}_1 = x_2
\dot{x}_2 = -x_1 + \epsilon \left(1 - x_1^2\right) x_2 + u, \epsilon > 0
y = x_1$$
(1)

- (a) Calculate the relative degree of the system.
- (b) Find a state feedback control law so that the equilibrium point at the origin of the closed-loop is globally asymptotically stable.

Solution:

(a)

$$\dot{y} = \dot{x}_1 = x_2 \tag{2}$$

$$\ddot{y} = \dot{x}_2 = -x_1 + \epsilon \left(1 - x_1^2\right) x_2 + u = \alpha(x) + \beta(x) u$$
 (3)

Therefore, the relative degree of the system is 2.

(b) The state feedback control law so that the equilibrium point at the origin of the closed-loop is globally asymptotically stable is shown as follows:

$$u = \frac{y_d^{(n)} - \sum_{i=1}^n \alpha_i e^{(n-i)} - \alpha(x)}{\beta(x)}$$

$$= -\alpha_1 \dot{e} - \alpha_2 e - \alpha(x)$$

$$= -\alpha_1 \dot{y} - \alpha_2 y - \alpha(x)$$

$$= -\alpha_1 x_2 - \alpha_2 x_1 + x_1 - \epsilon \left(1 - x_1^2\right) x_2$$
(4)

Because $\rho = n$, the closed-loop system can always be made an asymptotically stable linear system.

Choosing $\alpha_1 = 1$ and $\alpha_2 = 2$, the control law becomes

$$u = -x_2 - x_1 (5)$$

The motion equation of a single-link robot manipulator is given by

$$J\ddot{\theta} + MgL\sin\theta = u \tag{6}$$

- (a) Give the state space equation of (6) with $x_1 = \theta$, $x_2 = \dot{\theta}$, and $y = x_1$
- (b) Assume J = 5, gL = 1, and M = 10. Let $y_d(t)$ be a sufficiently smooth time function over $t \in [0, \infty)$. Let $e(t) = y(t) y_d(t)$. Design a state feedback control law so that e(t) satisfies $\ddot{e}(t) + 2\dot{e}(t) + e(t) = 0$.
- (c) Check your design in simple simulation for $y_d(t)$ to be a unit step input, and a sinusoidal function $\sin t$, respectively.

Solution:

(a) The state space equation of (6) with $x_1 = \theta$, $x_2 = \dot{\theta}$, and $y = x_1$ is shown as follows

$$\dot{x}_1 = x_2
\dot{x}_2 = -\frac{MgL\sin x_1}{J} + \frac{1}{J}u
y = x_1$$
(7)

(b) Because J = 5, gL = 1, and M = 10, the state space equation of (6) becomes

$$\dot{x}_1 = x_2
\dot{x}_2 = -2\sin x_1 + 0.2u
y = x_1$$
(8)

Then, we will find the relative degree ρ :

$$\dot{\mathbf{y}} = \dot{\mathbf{x}}_1 = \mathbf{x}_2 \tag{9}$$

$$\ddot{y} = \dot{x}_2 = -2\sin x_1 + 0.2u = \alpha(x) + \beta(x)u \tag{10}$$

Therefore, the relative degree of the system is 2. state feedback control law so that the system is globally asymptotically stable

$$u = \frac{y_d^{(n)} - \sum_{i=1}^n \alpha_i e^{(n-i)} - \alpha(x)}{\beta(x)}$$

$$= \frac{\ddot{y}_d(t) - \alpha_1 \dot{e}(t) - \alpha_2 e(t) - \alpha(x)}{\beta(x)}$$

$$= 5 (\ddot{y}_d(t) - \alpha_1 \dot{e}(t) - \alpha_2 e(t) + 2\sin x_1)$$
(11)

Substituting Equation (11) into Equation (10) obtains

$$\ddot{\mathbf{y}}(t) = \ddot{\mathbf{y}}_d(t) - \alpha_1 \dot{e}(t) - \alpha_2 e(t) \tag{12}$$

That is

$$\ddot{e}(t) + \alpha_1 \dot{e}(t) + \alpha_2 e(t) = 0 \tag{13}$$

Therefore, $\alpha_1 = 2$ and $\alpha_2 = 1$ can satisfy the requirements of $\ddot{e}(t) + 2\dot{e}(t) + e(t) = 0$. Hence, the state feedback control law is

$$u = 5 (\ddot{y}_d(t) - 2(x_2 - \dot{y}_d) - (x_1 - y_d) + 2\sin x_1)$$
(14)

(c) We use the following Simulink to get the results:

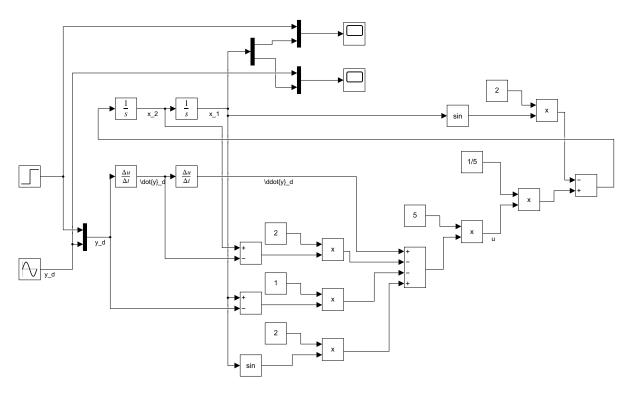


Figure 1: Block diagram for the system.

And we use the following code to plot the results:

```
1 clear all; clc;
2 figg1 = openfig('Q2Step.fig','reuse');
3 grid on;
4 xlabel('$t, \mathrm{\ \left(s\right)}$','interpreter','latex');
5 ylabel('$y, \mathrm{\ \left(m\right)}$', 'interpreter','latex');
6 legend('$y_d$', '$y$', 'interpreter','latex','Location','southeast');
7 title('');
8 a = get(gca,'XTickLabel');
9 set(gca,'XTickLabel',a,'FontName','Times','fontsize',12);
10 set(gcf,'renderer','painters');
11 filename = "Q2Step"+".pdf";
12 saveas(gcf,filename);
13 close(figg1);
14 figg2 = openfig('Q2Sine.fig','reuse');
```

```
15 grid on;
16 xlabel('$t, \mathrm{\ \left(s\right)}$','interpreter','latex');
17 ylabel('$y, \mathrm{\ \left(m\right)}$', 'interpreter','latex');
18 legend('$y_d$', '$y$', 'interpreter','latex','Location','southeast');
19 title('');
20 a = get(gca,'XTickLabel');
21 set(gca,'XTickLabel',a,'FontName','Times','fontsize',12);
22 set(gcf,'renderer','painters');
23 filename = "Q2Sine"+".pdf";
24 saveas(gcf,filename);
25 close(figg2);
```

The results are shown as follows:

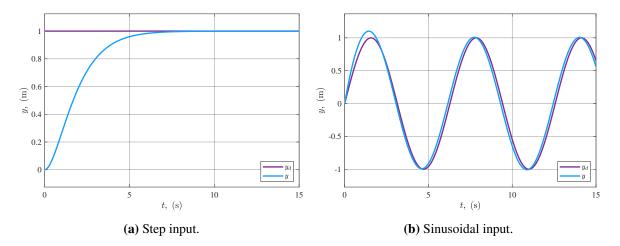


Figure 2: Simulation results.

Another way to achieve asymptotic tracking: Consider

$$y^{(n)} = \alpha(x) + \beta(x)u \tag{15}$$

or

$$\dot{x}_1 = x_2
\dots
\dot{x}_{n-1} = x_n
\dot{x}_n = \alpha(x) + \beta(x) u
y = x_1$$
(16)

where $x = \begin{bmatrix} y & \dot{y} & \cdots & y^{(n-1)} \end{bmatrix}$, $\alpha(x)$ and $\beta(x)$ are known and $\beta(x) \neq 0$ for all x. Given $y_d(t)$, let $e(t) = y(t) - y_d(t)$ and define

$$s = e^{(n-1)} + \alpha_1 e^{(n-2)} + \dots + \alpha_{n-1} e$$
 (17)

where $\alpha_1, ..., \alpha_{n-1}$ are such that

$$\lambda^{n-1} + \alpha_1 \lambda^{n-2} + \dots + \alpha_{n-2} \lambda + \alpha_{n-1}$$
 (18)

is a stable polynomial.

(a) Design a control law such that

$$\dot{s} + ks = 0 \tag{19}$$

where k > 0.

- (b) Show that the control law achieves $\lim_{t\to\infty} e(t) = 0$.
- (c) Show that, when $y_d = 0$, the closed-loop system is globally asymptotically stable.

Solution:

(a) To achieve asymptotic tracking for Equation (16), note that using an input transformation

$$\alpha(x) + \beta(x)u = u_a \tag{20}$$

or

$$u = \frac{u_a - \alpha(x)}{\beta(x)} \tag{21}$$

gives

$$y^{(n)} = u_a \tag{22}$$

which is in the chain integrator form. In order to achieve Equation (19) with $\rho = n$, i.e.,

$$(y^{(n)} - y_d^{(n)}) + (\alpha_1 + k) (y^{(n-1)} - y_d^{(n-1)}) + (\alpha_2 + k\alpha_1) (y^{(n-2)} - y_d^{(n-2)})$$

$$+ \dots + (\alpha_{n-1} + k\alpha_{n-2}) (y^{(1)} - y_d^{(1)}) + k\alpha_{n-1} (y - y_d) = 0$$

$$(23)$$

Substituting Equation (22) into (23) gives

$$\left(u_{a} - y_{d}^{(n)}\right) + (\alpha_{1} + k) \left(y^{(n-1)} - y_{d}^{(n-1)}\right) + (\alpha_{2} + k\alpha_{1}) \left(y^{(n-2)} - y_{d}^{(n-2)}\right)
+ ... + (\alpha_{n-1} + k\alpha_{n-2}) \left(y^{(1)} - y_{d}^{(1)}\right) + k\alpha_{n-1} \left(y - y_{d}\right) = 0$$

$$\implies u_{a} = y_{d}^{(n)} - \sum_{i=1}^{n} (\alpha_{i} + k\alpha_{i-1}) e^{n-i}$$
(24)

Here $\alpha_0 = 1$ and $\alpha_n = 0$. Thus,

$$u = \frac{u_a - \alpha(x)}{\beta(x)} = \frac{y_d^{(n)} - \sum_{i=1}^n (\alpha_i + k\alpha_{i-1}) e^{n-i} - \alpha(x)}{\beta(x)}$$
(25)

(b) Because

$$s = e^{(n-1)} + \alpha_1 e^{(n-2)} + \dots + \alpha_{n-1} e$$
 (26)

where $\alpha_1, ..., \alpha_{n-1}$ are such that

$$\lambda^{n-1} + \alpha_1 \lambda^{n-2} + \dots + \alpha_{n-2} \lambda + \alpha_{n-1}$$
 (27)

is a stable polynomial, for

$$\dot{s} = e^{(n)} + \alpha_1 e^{(n-1)} + \dots + \alpha_{n-1} e^{(1)}$$
(28)

where $\alpha_1, ..., \alpha_{n-1}$ are such that

$$\lambda^{n} + \alpha_{1}\lambda^{n-1} + \dots + \alpha_{n-2}\lambda^{2} + \alpha_{n-1}\lambda \tag{29}$$

is also a stable polynomial by Routh-Hurwitz stability criterion. Therefore,

$$\dot{s} + ks = e^{(n)} + (\alpha_1 + k) e^{(n-1)} + (\alpha_2 + k\alpha_1) e^{(n-2)} + \dots + (\alpha_{n-1} + k\alpha_{n-2}) e^{(1)} + k\alpha_{n-1}e = 0$$
(30)

where $\alpha_i + k\alpha_{i-1}$, i = 1, ..., n are such that

$$\lambda^{n} + (\alpha_{1} + k) \lambda^{n-1} + \dots + (\alpha_{n-1} + k\alpha_{n-2}) \lambda + k\alpha_{n-1}$$
(31)

is also a stable polynomial. As a result, e satisfies $\lim_{t\to\infty} e(t) = 0$.

(c) When $y_d = 0$, the closed-loop system is

$$\dot{x} = Ax + Bk (x, 0, ..., 0) = (A - B [k\alpha_{n-1}, (\alpha_{n-1} + k\alpha_{n-2}), ..., (\alpha_1 + k)]) x$$

$$= \begin{bmatrix}
0 & 1 & 0 & ... & 0 \\
0 & 0 & 1 & ... & 0 \\
... & & & & \\
0 & 0 & 0 & ... & 1 \\
-k\alpha_{n-1} - (\alpha_{n-1} + k\alpha_{n-2}) - (\alpha_{n-2} + k\alpha_{n-3}) & ... - (\alpha_1 + k)
\end{bmatrix} x$$
(32)

Clearly, $(A - B[k\alpha_{n-1}, (\alpha_{n-1} + k\alpha_{n-2}), ..., (\alpha_1 + k)])$ is a companion matrix with its characteristic polynomial being

$$\lambda^{n} + (\alpha_{1} + k) \lambda^{n-1} + \dots + (\alpha_{n-1} + k\alpha_{n-2}) \lambda + k\alpha_{n-1}$$
(33)

Thus, when $y_d = 0$, the closed-loop system is globally asymptotically stable.



THE CHINESE UNIVERSITY OF HONG KONG

DEPARTMENT OF MECHANICAL & AUTOMATION ENGINEERING

MAEG5070 Nonlinear Control Systems

Assignment #9

by

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Liuchao Gin

2022-23 Term 1

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Consider the following system

$$\dot{x}_1 = x_1 + x_2
\dot{x}_2 = x_3 + \cos(x_1)u
\dot{x}_3 = x_1 + x_2^2 + \lambda x_3
y = x_1$$
(1)

- (a) For what values of λ is the system minimum phase? nonminimum phase?
- (b) Assume a state feedback control law u = k(x) is such that $\ddot{y}(t) + 4\dot{y}(t) + 2y(t) = 0$. Is the equilibrium point at the origin of the closed-loop system (locally) asymptotically stable for all $\lambda \in R$? Why or Why not?

Solution:

(a) The Jacobian linearization of the system at the origin is given by

$$\dot{x} = Ax + Bu
y = Cx$$
(2)

with

$$A = \begin{bmatrix} 1 & 1 & 0 \\ 0 & 0 & 1 \\ 1 & 0 & \lambda \end{bmatrix}, \quad B = \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}, \quad C = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix}$$
 (3)

The transfer function of the above linear system is then given by

$$H(s) = C (sI - A)^{-1} B$$

$$= \frac{1}{s (s-1) (s-\lambda) + 1} C \begin{bmatrix} s (s-\lambda) & s-\lambda & 1\\ 1 & (s-1) (s-\lambda) & s-1\\ s & 1 & s (s-1) \end{bmatrix} B$$

$$= \frac{s-\lambda}{s (s-1) (s-\lambda) + 1}$$
(4)

The system has a zero at $s = \lambda$. Thus, it is minimum phase for all $\lambda < 0$ and it is nonminimum phase for all $\lambda \ge 0$.

(b) No. Since when $\lambda \geq 0$, the system is nonminimum phase at the origin, the equilibrium cannot be made locally asymptotically stable.

The motion equation of a single-link robot rigid-joint manipulator is given by

$$\ddot{y} + a\dot{y}\sin(y) = \beta(x)u \tag{5}$$

- (a) Give the state space equation of Equation (5) with $x_1 = y$ and $x_2 = \dot{y}$.
- (b) Assume $1 \le a \le 2$ and $0.5 < \beta(x) < 2.5$, using $\hat{a} = 1.5$ to design a sliding mode control law u such that

$$\frac{ds^2}{dt} \le -|s|\tag{6}$$

where $s = \dot{e} + 2e$ with $e = y - y_d$.

- (c) Assume y_d is a unit step function, simulate your design on the closed-loop system consisting of the plant Equation (5) with a=2 and the sliding mode control law with $\hat{a}=1.5$. Illustrate the performance of your control law by plotting y(t) and $y_d(t)$ in the same figure for $0 \le t \le 20$. Also, plot u(t) for $0 \le t \le 20$.
- (d) In the control law designed in part (b), replace sgn(s) by sat(s/0.2), and repeat part (c). Hint: In simulation, you can let $F(x) = |\alpha(x) \hat{\alpha}(x)|$ and $\beta(x) = 1$. **Solution:**
 - (a) Let $x_1 = y$ and $x_2 = \dot{y}$, the state-space equation is

$$\begin{cases} \dot{x}_1 = x_2 \\ \dot{x}_2 = -ax_2 \sin x_1 + \beta(x) u \\ y = x_1 \end{cases}$$
 (7)

(b) Define the estimate $\hat{\beta}$ of $\beta(x)$ by $\hat{\beta} = (b_{min}b_{max})^{1/2} = \frac{\sqrt{5}}{2}$ and let $b = (b_{max}/b_{min})^{1/2} = \sqrt{5}$.

Using $\hat{a} = 1.5$ yields that

$$\hat{\alpha} = -1.5x_2 \sin x_1 \tag{8}$$

$$\Delta \alpha = \alpha (x) - \hat{\alpha} \Longrightarrow |\Delta \alpha| = |\alpha (x) - \hat{\alpha}| \le 0.5 |x_2 \sin x_1| \Longrightarrow F(x) = 0.5 |x_2 \sin x_1| \quad (9)$$

Therefore,

$$\hat{u} = -\hat{\alpha}(x) + \ddot{y}_d - \alpha_1 \dot{e} \tag{10}$$

Because $s = \dot{e} + 2e$, $\alpha_1 = 2$. Therefore,

$$\hat{u} = 1.5x_2 \sin x_1 + \ddot{y}_d - 2\dot{e} \tag{11}$$

Because the sliding mode control law u should satisfy

$$\frac{ds^2}{dt} \le -|s|\tag{12}$$

we can know that $\eta = \frac{1}{2}$. Therefore, we can let $\phi(x)$ be

$$\phi(x) = b (F(x) + \eta) + (b - 1) |\hat{u}|$$

$$= \sqrt{5} \left(0.5 |x_2 \sin x_1| + \frac{1}{2} \right) + \left(\sqrt{5} - 1 \right) |1.5x_2 \sin x_1 + \ddot{y}_d - 2\dot{e}|$$

$$= \sqrt{5} \left(0.5 |x_2 \sin x_1| + \frac{1}{2} \right) + \left(\sqrt{5} - 1 \right) |1.5x_2 \sin x_1 + \ddot{y}_d - 2 (\dot{y} - \dot{y}_d)|$$

$$= \sqrt{5} \left(0.5 |x_2 \sin x_1| + \frac{1}{2} \right) + \left(\sqrt{5} - 1 \right) |1.5x_2 \sin x_1 + \ddot{y}_d - 2 (x_2 - \dot{y}_d)|$$

$$= \sqrt{5} \left(0.5 |x_2 \sin x_1| + \frac{1}{2} \right) + \left(\sqrt{5} - 1 \right) |1.5x_2 \sin x_1 + \ddot{y}_d - 2 (x_2 - \dot{y}_d)|$$
(13)

Hence, we can design a sliding mode control law u as follows:

$$u = \hat{\beta}^{-1} \left[\hat{u} - \phi(x) \, sgn(s) \right]$$

$$= \frac{2}{\sqrt{5}} \left[1.5x_2 \sin x_1 + \ddot{y}_d - 2\dot{e} - \phi(x) \, sgn(s) \right]$$

$$= \frac{2}{\sqrt{5}} \left[1.5x_2 \sin x_1 + \ddot{y}_d - 2(x_2 - \dot{y}_d) - \phi(x) \, sgn(s) \right]$$
(14)

where

$$\phi(x) = \sqrt{5} \left(0.5 |x_2 \sin x_1| + \frac{1}{2} \right) + \left(\sqrt{5} - 1 \right) |1.5x_2 \sin x_1 + \ddot{y}_d - 2 (x_2 - \dot{y}_d)|$$
 (15)

$$s = \dot{e} + 2e = (\dot{y} - \dot{y}_d) + 2(y - y_d) = (x_2 - \dot{y}_d) + 2(x_1 - y_d)$$
(16)

The MATLAB shown below is used to simulate the performance of the designed controller.

```
1 clc; clf; clear all;
2 %% sgn part
3 [t,x] = ode45('Q9_2_Systemsgn',[0,20],[0 0]);
4 phi = 0.5+0.5*abs(x(:,2).*sin(x(:,1)));
5 y_d = 1;
6 \text{ y\_ddot} = 0;
7 y \text{ dddot} = 0;
8 y = x(:,1);
9 ydot = x(:,2);
10 s = ydot-y_ddot+2*(y-y_d);
11 u = -phi.*sgn(s)+1.5*x(:,2).*sin(x(:,1))+y_dddot-2*(ydot-y_ddot);
12 figure(1);
13 hold on;
14 plot(t, y,'color',[0.667 0.667 1],'LineWidth',2.5);
15 plot(t, y_d+t*0,'color',[1 0.5 0],'LineWidth',2.5);
16 hold off;
17 grid on;
18 legend('$y\left(t\right)$','$y d\left(t\right)$','interpreter','latex');
19 xlabel('$t, \ (\mathrm{s})$','interpreter','latex');
20 ylabel('$\theta, \ (\mathrm{rad})$','interpreter','latex');
21 a = get(gca,'XTickLabel');
22 set(gca,'XTickLabel',a,'FontName','Times','fontsize',12);
```

```
23 set(gca, 'position', [0.15 0.20 0.6 0.6]);
24 set(gcf, 'position', [100 100 800 600]);
25 set(gcf,'renderer','painters');
26 filename = "Q9-2-yyd-sgn"+".pdf";
27 saveas (gcf, filename);
28 figure(2);
29 plot(t, u,'color',[0.667 0.667 1],'LineWidth',2.5);
30 grid on;
31 xlabel('$t, \ (\mathrm{s})$','interpreter','latex');
32 ylabel('$u, \ (\mathrm{N\cdot m})$','interpreter','latex');
33 a = get(gca,'XTickLabel');
34 set(gca,'XTickLabel',a,'FontName','Times','fontsize',12);
35 set(gca, 'position', [0.15 0.20 0.6 0.6]);
36 set(gcf, 'position', [100 100 800 600]);
37 set(gcf,'renderer','painters');
38 filename = "Q9-2-u-sgn"+".pdf";
39 saveas (gcf, filename);
40 %% sat part
41 [t,x] = ode45('Q9_2_Systemsat', [0,20], [0 0]);
42 phi = 0.5+0.5*abs(x(:,2).*sin(x(:,1)));
43 \quad y_d = 1;
44 y_dot = 0;
45 y_dddot = 0;
46 y = x(:,1);
47 ydot = x(:,2);
48 s = ydot-y_ddot+2*(y-y_d);
49 u = -phi.*sgn(s)+1.5*x(:,2).*sin(x(:,1))+y_dddot-2*(ydot-y_ddot);
50 figure(3);
51 hold on;
52 plot(t, y,'color',[0.667 0.667 1],'LineWidth',2.5);
53 plot(t, y_d+t*0,'color',[1 0.5 0],'LineWidth',2.5);
54 hold off;
55 grid on;
56 legend('$y\left(t\right)$','$y_d\left(t\right)$','interpreter','latex');
57 xlabel('$t, \ (\mathrm{s})$','interpreter','latex');
58 ylabel('$\theta, \ (\mathrm{rad})$','interpreter','latex');
59 a = get(gca,'XTickLabel');
60 set(gca,'XTickLabel',a,'FontName','Times','fontsize',12);
61 set(gca, 'position', [0.15 0.20 0.6 0.6]);
62 set(gcf, 'position', [100 100 800 600]);
63 set(gcf,'renderer','painters');
64 filename = "Q9-2-yyd-sat"+".pdf";
65 saveas (gcf, filename);
66 figure(4);
67 plot(t, u,'color',[0.667 0.667 1],'LineWidth',2.5);
68 grid on;
```

where the codes for the system representation are shown below:

```
1 function xd = Q9_2_Systemsgn(t,x)
2
        xd(1) = x(2);
3
       phi = 0.5+0.5*abs(x(2)*sin(x(1)));
4
       y_d = 1;
       y_ddot = 0;
5
6
       y_dddot = 0;
7
       y = x(1);
8
       ydot = x(2);
9
        s = ydot-y_ddot+2*(y-y_d);
10
       u = -phi * sqn(s) + 1.5 * x(2) * sin(x(1)) + y_dddot - 2 * (ydot - y_ddot);
        xd(2) = -2*x(2)*sin(x(1))+u;
11
12
        xd = xd';
13 end
```

and the sgn function is designed as follows:

```
function y = sgn(s)

if s == 0

y = 0;

else

y = s./abs(s);

end

end
```

The simulation results are shown in Figure 1.

(c) The codes for the controller are changed for sat function as shown below:

```
1 function xd = Q9_2_Systemsat(t,x)
2     xd(1) = x(2);
3     phi = 0.5+0.5*abs(x(2)*sin(x(1)));
4     y_d = 0*t+1;
5     y_ddot = 0;
6     y_dddot = 0;
7     y = x(1);
8     ydot = x(2);
```

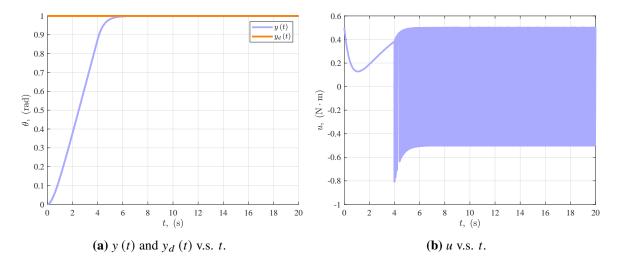


Figure 1: Simulation results for the controller with sgn.

and the sat function is designed as follows:

```
function y = sat(s)
1
2
       if abs(s) < 0.2
3
            y = s;
4
       elseif s < 0</pre>
5
            y = -1;
6
       else
7
            y = 1;
8
       end
9
  end
```

The simulation results are shown in Figure 2.

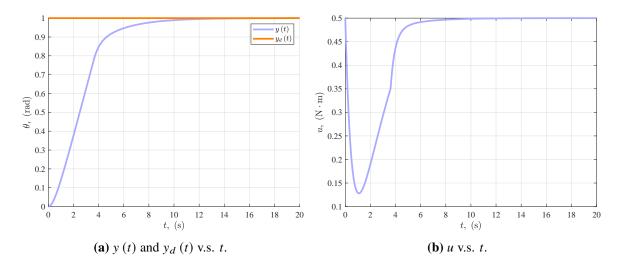


Figure 2: Simulation results for the controller with sat.

Consider the motion equation of a single-link robot rigid-joint manipulator given in Equation (5) where $\beta(x) = 1$ for all x.

- (a) Assume a = 1.5, $y_d = 2 \sin t$ and $s = \dot{e} + 3e$. Design a control law of the form (8.7) of the lecture note with k = 2 and simulate the performance of your control law by plotting y(t) and $y_d(t)$ in the same figure for $0 \le t \le 20$. Also, plot u(t) for $0 \le t \le 20$.
- (b) Assume the actual value of a=2. Use the same control law as the one in Part (i) to simulate the performance of your control law by plotting y(t) and $y_d(t)$ in the same figure for $0 \le t \le 20$. Also, plot u(t) for $0 \le t \le 20$.
- (c) Assume a is unknown, put the system in the form (8.3) of the lecture note and identify a_0 , a_1 , a_2 and f_1 , f_2 .
- (d) Design an adaptive control law of the form (8.10) and (8.12) of the lecture note with $\gamma_i = 3$. Assume the actual value of a = 2.5, respectively. Simulate the performance of your control law by plotting y(t) and $y_d(t)$ in the same figure for $0 \le t \le 20$. Also, plot u(t) and $\hat{a}_i(t)$ for $0 \le t \le 20$.

Hint: Note Part (iv) of Remark 8.1.

Solution:

(a) Because $\beta(x) = 1$, $a_0 = 1$. Consider the control law,

$$u = a_0 f_0(x, t) - ks + \sum_{i=1}^{m} a_i f_i(x, t)$$
(17)

where k = 2, and

$$f_0(x,t) = \ddot{y}_d - \alpha_1 \dot{e} \tag{18}$$

Because $s = \dot{e} + 3e$, $\alpha_1 = 3$. Therefore, the designed control law for the system is as follows:

$$u = \ddot{y}_d - 3\dot{e} - 2s + 1.5\dot{y}\sin(y)$$

= $\ddot{y}_d - 3(x_2 - \dot{y}_d) - 2((x_2 - \dot{y}_d) + 3(x_1 - y_d)) + 1.5x_2\sin x_1$ (19)

The MATLAB shown below is used to simulate the performance of the designed controller.

```
1 clc; clf; clear all;
2 %% Q9-3-a
3 [t,x] = ode45('Q9_3_a_System',[0,20],[0 0]);
4 y_d = 2*sin(t);
5 y_ddot = 2*cos(t);
6 y_dddot = -2*sin(t);
```

```
7 y = x(:,1);
 8 ydot = x(:,2);
9 s = ydot-y_ddot+3*(y-y_d);
10 \ a0 = 1;
11 f0 = y_dddot-3*(ydot-y_ddot);
12 u = a0*f0-2*s+1.5*x(:,2).*sin(x(:,1));
13 figure(1);
14 hold on;
15 plot(t, y,'color',[0.667 0.667 1],'LineWidth',2.5);
16 plot(t, y_d+t*0,'color',[1 0.5 0],'LineWidth',2.5);
17 hold off;
18 grid on;
19 legend('$y\left(t\right)$','$y_d\left(t\right)$','interpreter','latex');
20 xlabel('$t, \ (\mathrm{s})$','interpreter','latex');
21 ylabel('$\theta, \ (\mathrm{rad})$','interpreter','latex');
22 a = get(gca,'XTickLabel');
23 set(gca,'XTickLabel',a,'FontName','Times','fontsize',12);
24 set(gca, 'position', [0.15 0.20 0.6 0.6]);
25 set(gcf, 'position', [100 100 800 600]);
26 set(gcf,'renderer','painters');
27 filename = "Q9-3-a-yyd"+".pdf";
28 saveas (gcf, filename);
29 figure(2);
30 plot(t, u,'color',[0.667 0.667 1],'LineWidth',2.5);
31 grid on;
32 xlabel('$t, \ (\mathrm{s})$','interpreter','latex');
33 ylabel('$u, \ (\mathrm{N\cdot m})$','interpreter','latex');
34 a = get(gca,'XTickLabel');
35 set(gca, 'XTickLabel', a, 'FontName', 'Times', 'fontsize', 12);
36 set(gca, 'position', [0.15 0.20 0.6 0.6]);
37 set(gcf,'position',[100 100 800 600]);
38 set(gcf,'renderer','painters');
39 filename = "Q9-3-a-u"+".pdf";
40 saveas (gcf, filename);
41 %% Q9-3-b
42 [t,x] = ode45('Q9_3_b_System', [0,20], [0 0]);
43 y_d = 2*sin(t);
44 y_{dot} = 2*cos(t);
45 y_dddot = -2*sin(t);
46 y = x(:,1);
47 ydot = x(:,2);
48 s = ydot-y_dot+3*(y-y_d);
49 \quad a0 = 1;
50 	 f0 = y_dddot-3*(ydot-y_ddot);
51 u = a0*f0-2*s+1.5*x(:,2).*sin(x(:,1));
52 figure(3);
```

```
53 hold on;
54 plot(t, y,'color',[0.667 0.667 1],'LineWidth',2.5);
55 plot(t, y_d+t*0,'color',[1 0.5 0],'LineWidth',2.5);
56 hold off;
57 grid on;
58 legend('$y\left(t\right)$','$y_d\left(t\right)$','interpreter','latex');
59 xlabel('$t, \ (\mathrm{s})$','interpreter','latex');
60 ylabel('$\theta, \ (\mathrm{rad})$','interpreter','latex');
61 a = get(gca,'XTickLabel');
62 set(gca,'XTickLabel',a,'FontName','Times','fontsize',12);
63 set(gca, 'position', [0.15 0.20 0.6 0.6]);
64 set(gcf,'position',[100 100 800 600]);
65 set(gcf,'renderer','painters');
66 filename = "Q9-3-b-yyd"+".pdf";
67 saveas (gcf, filename);
68 figure(4);
69 plot(t, u,'color',[0.667 0.667 1],'LineWidth',2.5);
70 grid on;
71 xlabel('$t, \ (\mathrm{s})$','interpreter','latex');
72 ylabel('$u, \ (\mathrm{N\cdot m})$','interpreter','latex');
73 a = get(gca,'XTickLabel');
74 set(gca,'XTickLabel',a,'FontName','Times','fontsize',12);
75 set(gca, 'position', [0.15 0.20 0.6 0.6]);
76 set(gcf, 'position', [100 100 800 600]);
77 set(gcf,'renderer','painters');
78 filename = "Q9-3-b-u"+".pdf";
79 saveas(gcf, filename);
```

where the codes for the system representation are shown below:

```
1 function xd = Q9_3_a_System(t,x)
2
       xd(1) = x(2);
3 %
        phi = 0.5+0.5*abs(x(2)*sin(x(1)));
4
       y_d = 2*sin(t);
5
       y_{dot} = 2*cos(t);
6
       y_{dddot} = -2*sin(t);
7
       y = x(1);
8
       ydot = x(2);
9
       s = ydot-y_ddot+3*(y-y_d);
10
       a0 = 1;
11
       f0 = y_dddot-3*(ydot-y_ddot);
12
       u = a0*f0-2*s+1.5*x(2)*sin(x(1));
13
       xd(2) = -1.5*x(2)*sin(x(1))+u;
14
       xd = xd';
15 end
```

The simulation results are shown in Figure 3.

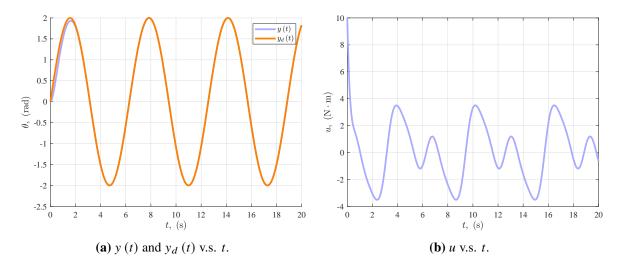


Figure 3: Simulation results for the controller with for the adaptive control with k = 2.

(b) The codes for the system representation are changed as shown below:

```
function xd = Q9_3_b_System(t,x)
2
       xd(1) = x(2);
         phi = 0.5+0.5*abs(x(2)*sin(x(1)));
3
4
       y_d = 2*sin(t);
5
       y_{dot} = 2*cos(t);
       y_dddot = -2*sin(t);
6
7
       y = x(1);
8
       ydot = x(2);
9
       s = ydot-y_ddot+3*(y-y_d);
10
       a0 = 1;
11
       f0 = y_dddot-3*(ydot-y_ddot);
       u = a0*f0-2*s+1.5*x(2)*sin(x(1));
12
       xd(2) = -2*x(2)*sin(x(1))+u;
13
14
       xd = xd';
15
   end
```

The simulation results are shown in Figure 4.

(c)
$$a_0 y^{(n)} + \sum_{i=1}^m a_i f(x, t) = u$$
 (20)

Here, $a_0 = 1$, $a_1 = a$, $a_2 = 0$, $f_1(x) = x_2 \sin x_1$, $f_2(x) = 0$

(d)

$$u = a_0 f_0(x, t) - ks + \sum_{i=1}^{m} \hat{a}_i f_i(x, t)$$

$$\dot{\hat{a}}_i = -\gamma_i sgn(a_0) sf_i, i = 1, \dots, m$$
(21)

Because $\gamma_i = 3$ and $a_0 = 1$, Equation (21) can be simplified into

$$u = (\ddot{y}_d - 3(x_2 - \dot{y}_d)) - 2((x_2 - \dot{y}_d) + 3(x_1 - y_d)) + \hat{a}_1 x_2 \sin x_1$$

$$\dot{a}_1 = -3((x_2 - \dot{y}_d) + 3(x_1 - y_d)) x_2 \sin x_1$$
(22)

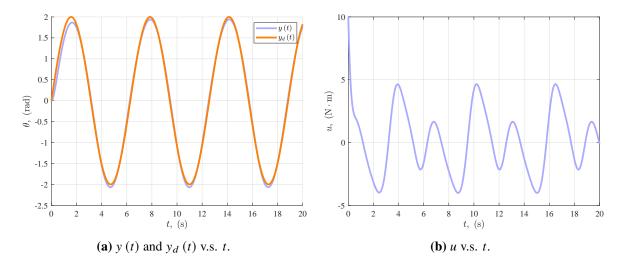


Figure 4: Simulation results for the controller with for the adaptive control with k=2 and the actual value of a=2.

The Simulink as shown in Figure 5 is used to simulate the performance of the designed controller.

And we use the following code to plot the results:

```
1 clear all; clc;
2 figg1 = openfig('Q9-3-d-ahat.fig','reuse');
3 grid on;
4 xlabel('$t, \mathrm{\ \left(s\right)}$','interpreter','latex');
5 ylabel('$\hat{a}$', 'interpreter','latex');
6 % legend('$y_d$', '$y$', 'interpreter','latex','Location','southeast');
7 title('');
8 a = get(gca,'XTickLabel');
9 set(gca,'XTickLabel',a,'FontName','Times','fontsize',12);
10 set(gca, 'position', [0.15 0.20 0.6 0.6]);
11 set(gcf,'position',[100 100 800 600]);
12 set(gcf, 'renderer', 'painters');
13 filename = "Q9-3-d-ahat"+".pdf";
14 saveas(gcf, filename);
15 close(figg1);
16 figg2 = openfig('Q9-3-d-u.fig','reuse');
17 grid on;
18 \times \lim([0.07 20]);
19 ylim([-5 6]);
20 xlabel('$t, \ (\mathrm{s})$','interpreter','latex');
21 ylabel('$u, \ (\mathrm{N\cdot m})$','interpreter','latex');
22 % legend('$y_d$', '$y$', 'interpreter', 'latex', 'Location', 'southeast');
23 title('');
24 a = get(gca,'XTickLabel');
25 set(gca,'XTickLabel',a,'FontName','Times','fontsize',12);
26 set(gca, 'position', [0.15 0.20 0.6 0.6]);
```

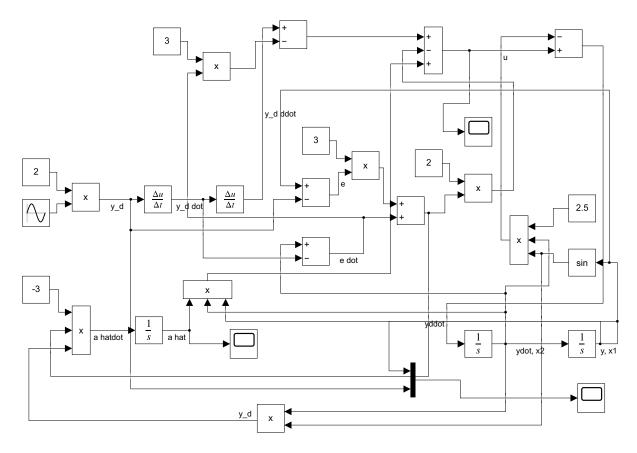


Figure 5: Block diagram for the system.

```
27 set(gcf,'position',[100 100 800 600]);
28 set(gcf,'renderer','painters');
29 filename = "Q9-3-d-u"+".pdf";
30 saveas (gcf, filename);
31 close(figg2);
32 figg3 = openfig('Q9-3-d-yyd.fig','reuse');
33 grid on;
34 legend('$y\left(t\right)$','$y_d\left(t\right)$','interpreter','latex');
35 xlabel('$t, \ (\mathrm{s})$','interpreter','latex');
36 ylabel('$\theta, \ (\mathrm{rad})$','interpreter','latex');
37 title('');
38 a = get(gca,'XTickLabel');
39 set(gca,'XTickLabel',a,'FontName','Times','fontsize',12);
40 set(gca, 'position', [0.15 0.20 0.6 0.6]);
41 set(gcf, 'position', [100 100 800 600]);
42 set(gcf,'renderer','painters');
43 filename = "Q9-3-d-yyd"+".pdf";
44 saveas (gcf, filename);
45 close(figg3);
```

The simulation results are shown in Figure 6.

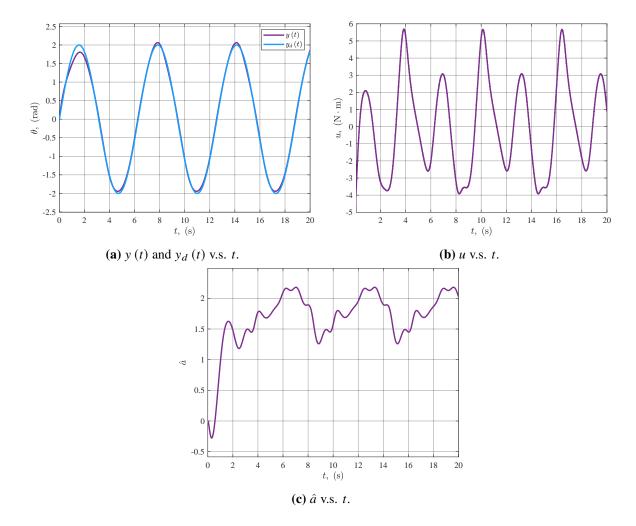


Figure 6: Simulation results for the controller with for the adaptive control law of the form (8.10) and (8.12) of the lecture note.